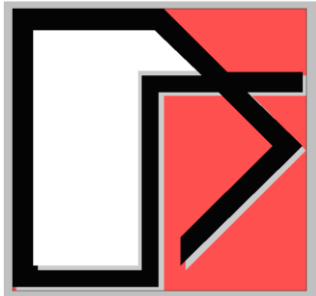


SEISMIC SSI ANALYSIS OF RB COMPLEX ON PILE FOUNDATION INCLUDING SOIL NONLINEAR HYSTERETIC BEHAVIOR



Ghiocel Predictive Technologies Inc.

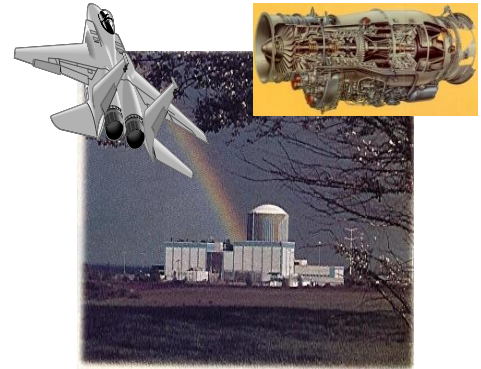
Dr. Dan M. Ghiocel

Member of ASCE 4 & 43 Standards

Email: dan.ghiocel@ghiocel-tech.com

Ghiocel Predictive Technologies Inc.

<http://www.ghiocel-tech.com>



DOE/NRC Natural Phenomena Hazards Meeting

October 20-22, 2020

Purpose of Presentation:

To investigate SSI effects for a NI complex founded on piles.

Both floating piles (Case A) and peak-bearing piles (Case B) are considered.

Investigate the effects of

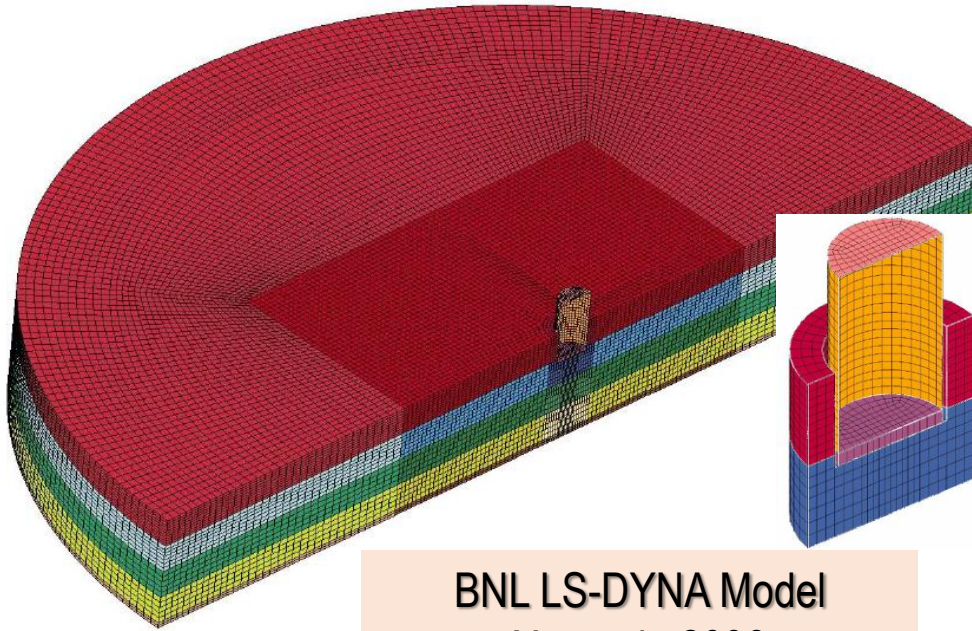
- Floating piles (Case A) vs. peak-bearing piles (Case B)
- Motion spatial variation effects (incoherency and inclined waves)
- Local nonlinear soil behaviour in the vicinity of piles.

Used the ACS SASSI V4.1 software

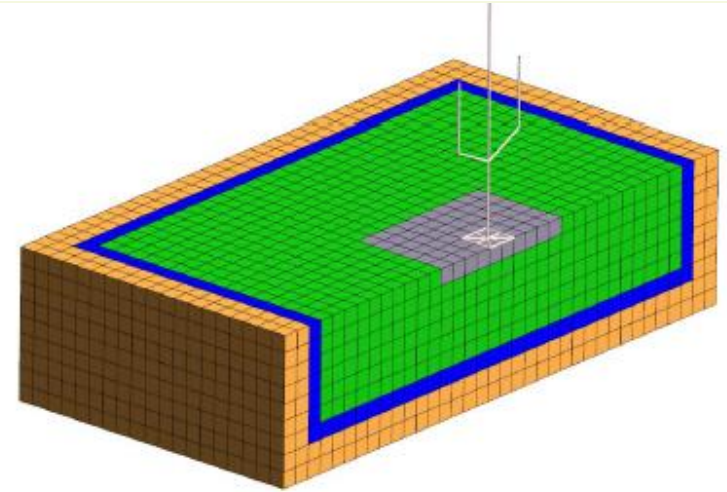
1. Application of SASSI Methodology

- Nonlinear Soil Behavior in Vicinity of Foundations
- Excavated Soil Modeling (Mesh and Interaction Nodes)

Direct SSI Approach and SASSI Approach

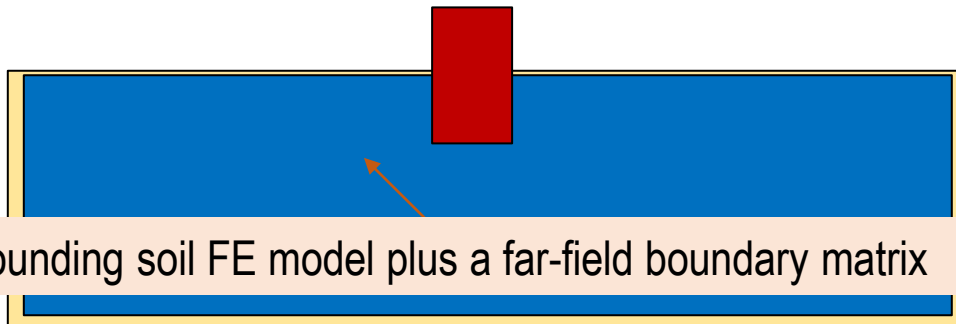


BNL LS-DYNA Model
Xu et al., 2006



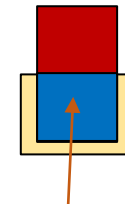
E-SSI Model
Neboja et al., 2015

Time-Domain SSI Approach



Surrounding soil FE model plus a far-field boundary matrix

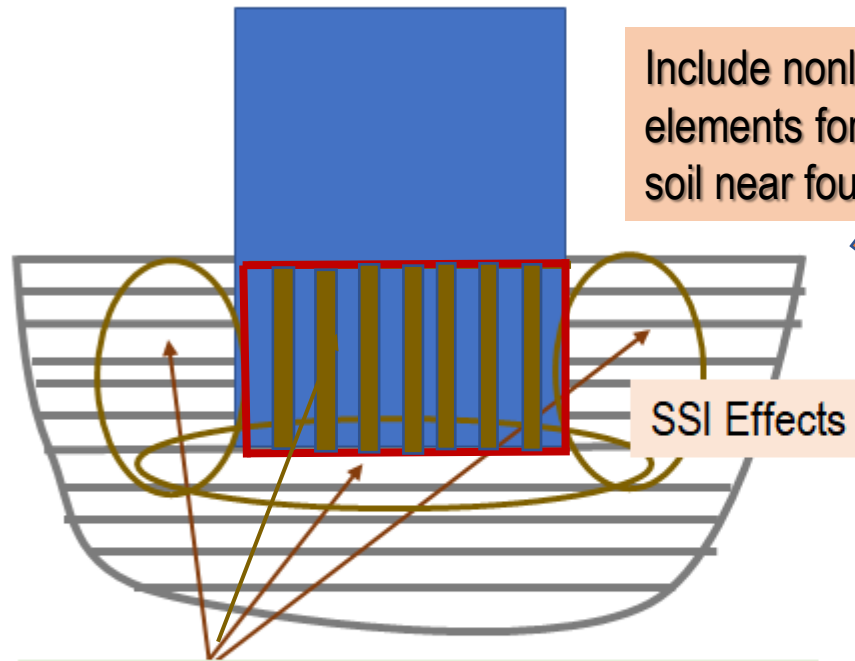
SASSI Approach



Excavated soil FE model plus the far-field soil impedance matrix

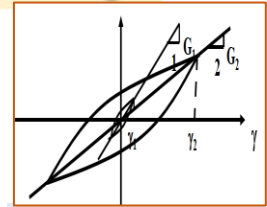
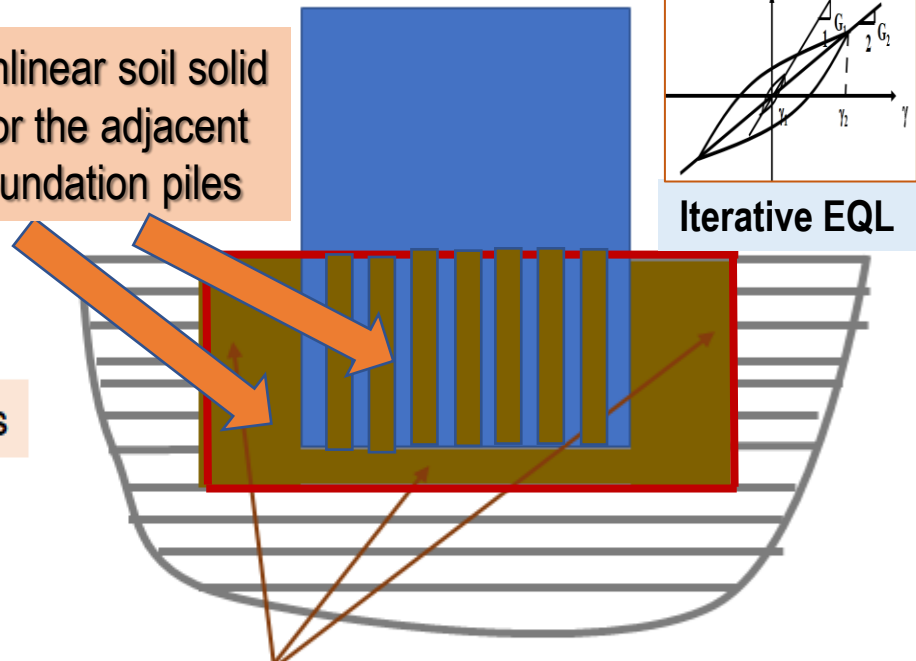
Improving SASSI Modeling By Including Pile Foundation Adjacent Soil Hysteretic Behavior

"Standard" SASSI Modeling



Typically, SSI model uses in the vicinity of foundation iterated strain-compatible soil layer properties computed using iterative 1D wave propagation equivalent-linear approach, *EQL via SHAKE methodology*. SSI effects on soil behavior are neglected.

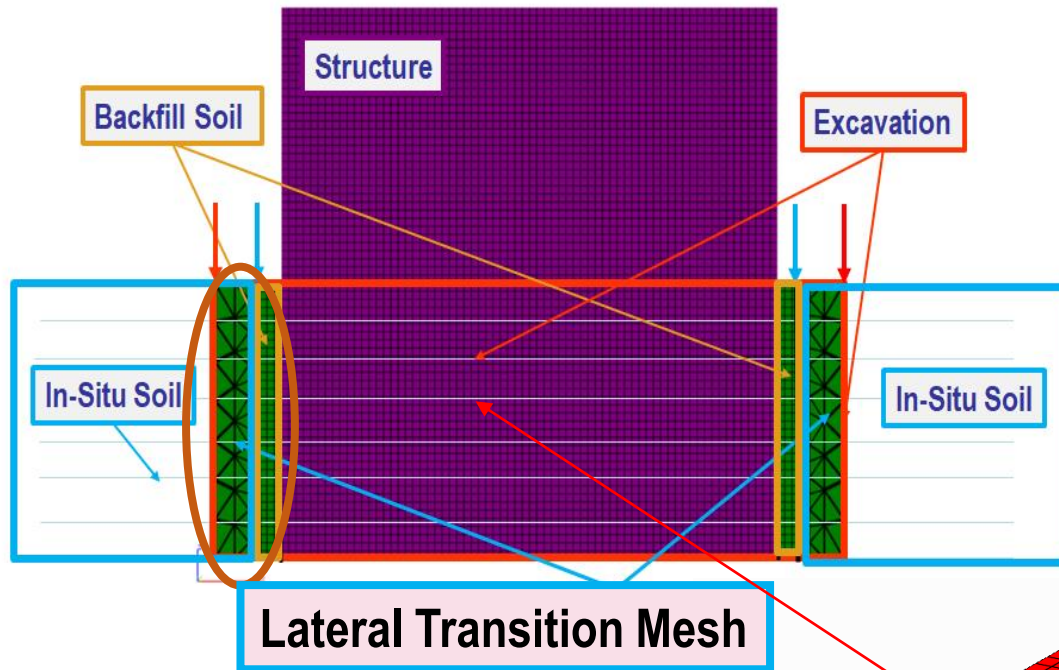
"Improved" SASSI Modeling



Iterative EQL

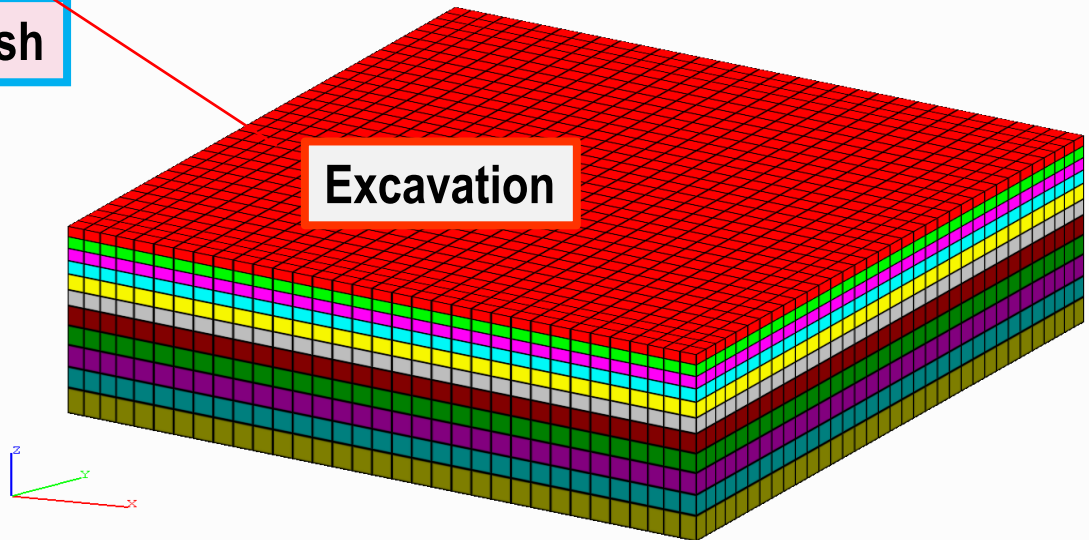
SSI model uses in the vicinity of foundation iterated strain-compatible soil layer properties computed using iterative 3D SASSI equivalent-linear approach to capture SSI effects, *EQL via fast SASSI iterations*.

Transition Mesh Zone Is Needed to Connect Pile Foundation Mesh with Excavation Mesh



Regular mesh excavated soil FE models capture accurately the high-frequency wave scattering effects and also ensures more efficient SSI runs (less inter. nodes).
See conclusions of the Brookhaven National Lab Report BNL-102434 by USNRC BNL Consultants (Nie et al., 2013)

Excavation mesh should be a regular, structured mesh to provide accurate wave scattering results, and also use MSM approach.

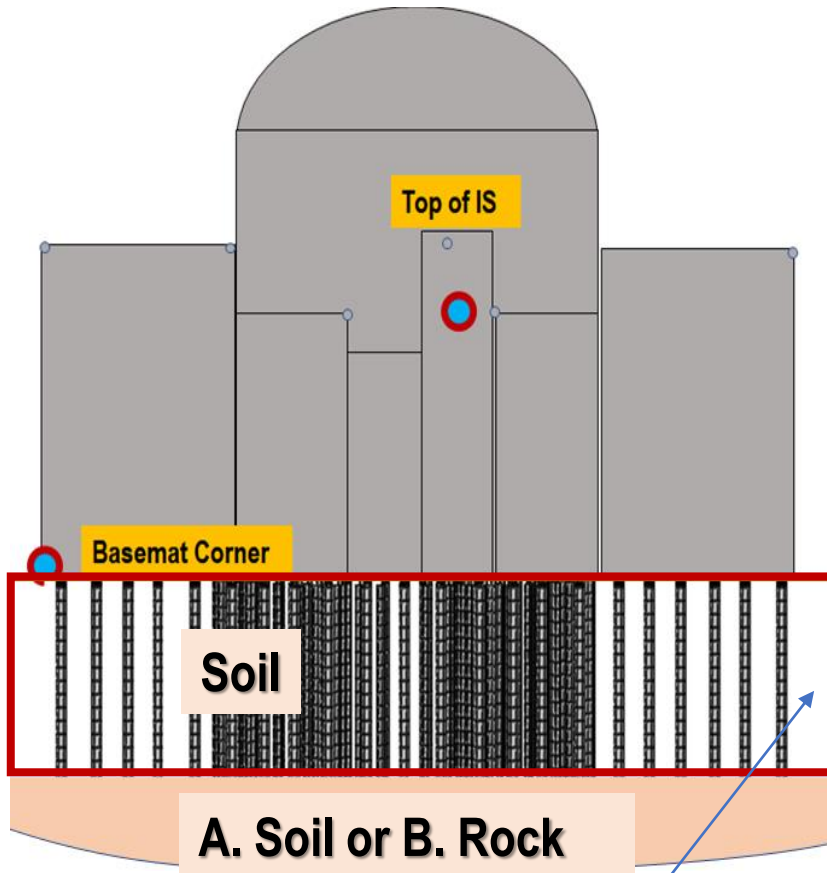


2. RB Complex on Pile Foundation Sensitivity Study

- Floating Pile (FP) vs. Peak Bearing Pile (PBP)
- Coherent vs. Incoherent Seismic Input Motions
- Nonlinear vs. Linear Soil Behavior in Vicinity of Piles

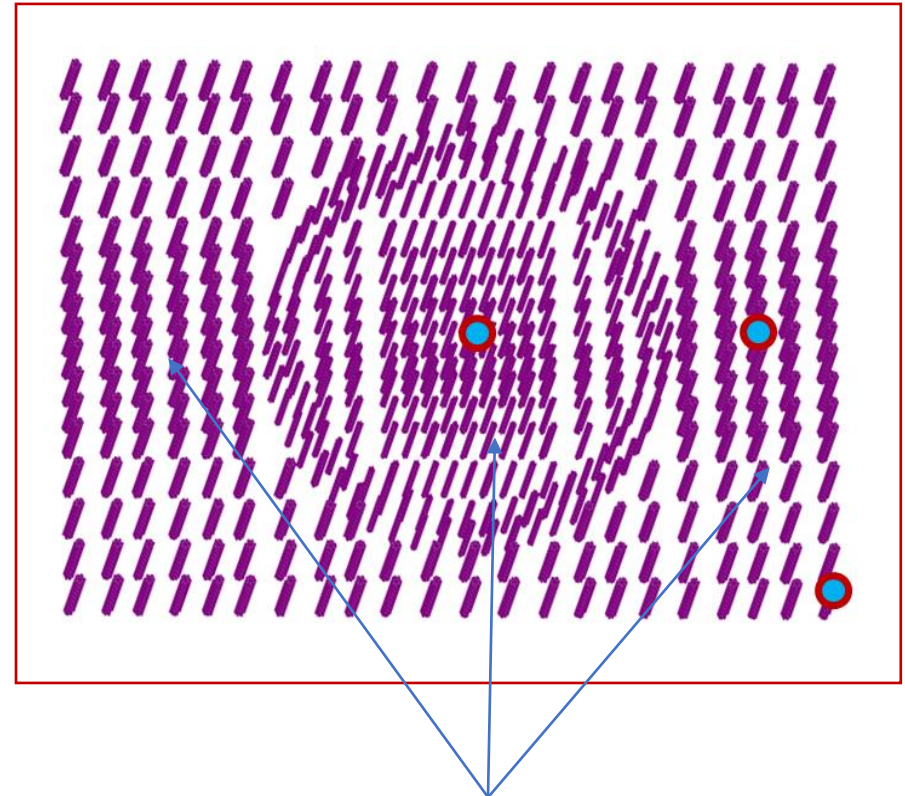
SSI Modeling of RB Complex on Pile Foundation

RB Complex on Piles



Excavated soil has a much larger horizontal size than vertical size. Efficient MSM is applicable.

Pile Foundation (about 500 piles)

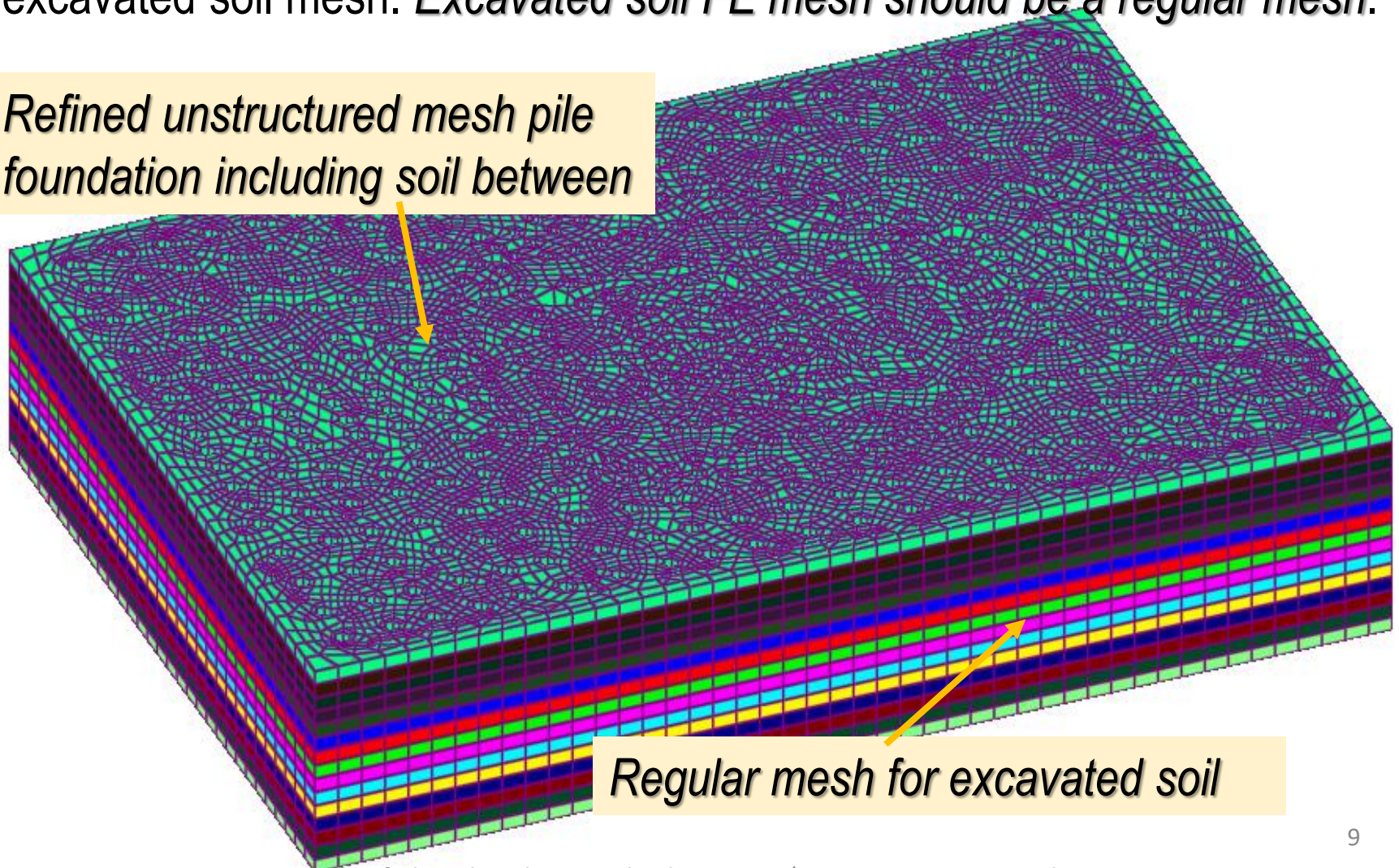


Pile diameter and density varies;
D1=1m diameter, D2=1.5m diameter

RB Complex Pile Foundation Modeling

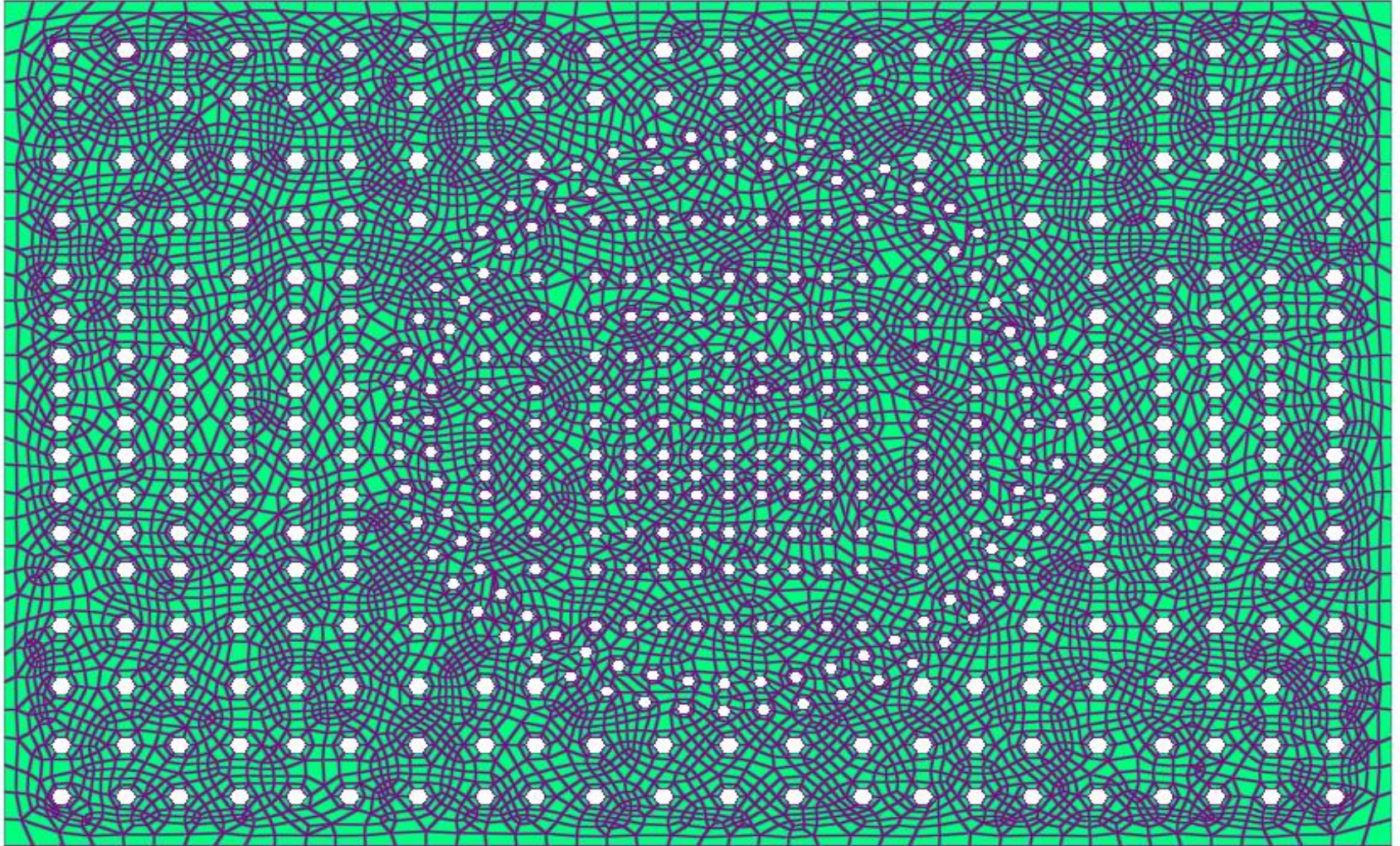
The soil *FE* mesh is refined and unstructured between piles, but it should be coarser and regular at the mesh boundaries were connected to the excavated soil mesh. *Excavated soil FE mesh should be a regular mesh.*

Refined unstructured mesh pile foundation including soil between



Regular mesh for excavated soil

RB Complex Pile Foundation Modeling



This pile foundation SASSI modelling provides a high numerical efficiency. MSM is applicable. The SSI model of about 250,000 nodes was run on a 256GB RAM PC under MS Window 10 in about 20 hours for 100 SSI frequencies (w/ ACS SASSI V4 software).

Other SSI Modeling Aspects

Foundation Basemat Connection with Piles

The RB complex basemat is assumed with no embedment and sitting only on the concrete piles. It was assumed that the basemat was not directly transmitting any load pressures to the surrounding soil.

This SSI modelling avoids on purpose including the potential basemat contribution to the overall pile foundation impedance.

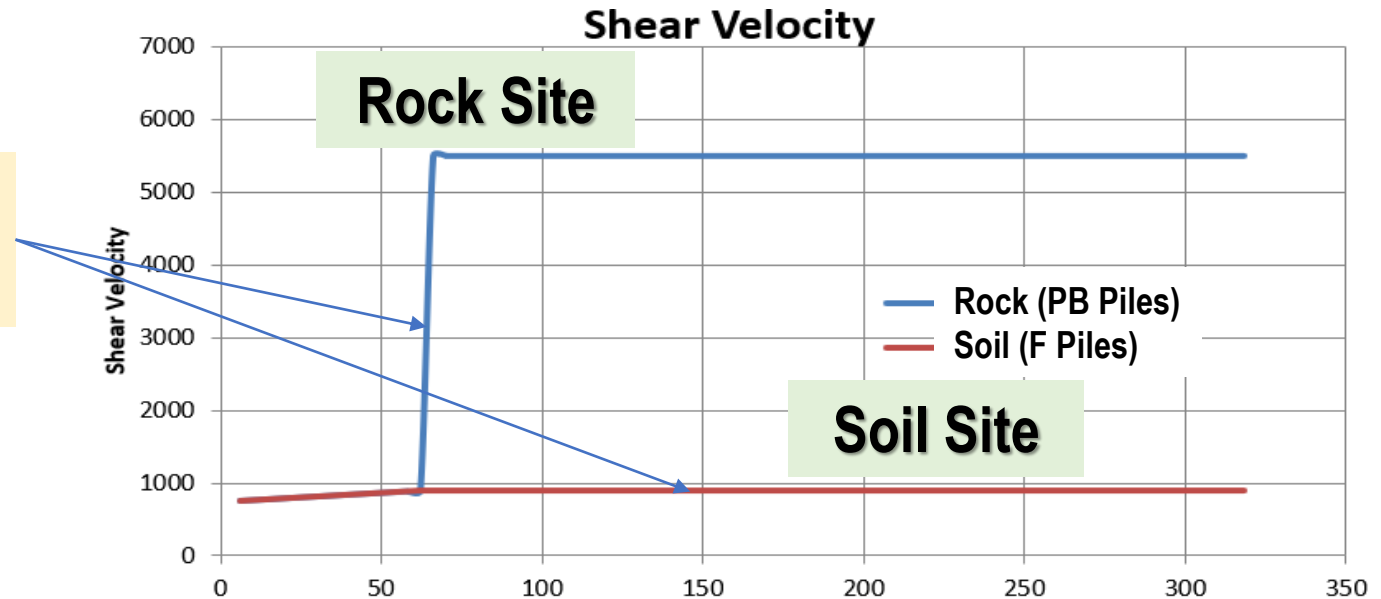
Nonlinear Soil Behaviour in Vicinity of Piles

A highly efficient global-local SSI analysis was used based on computing iteratively the SSI response for the equivalent-linearized system in complex frequency, and, then, for each soil element the local nonlinear soil behaviour in time domain for the simultaneous X, Y and Z inputs.

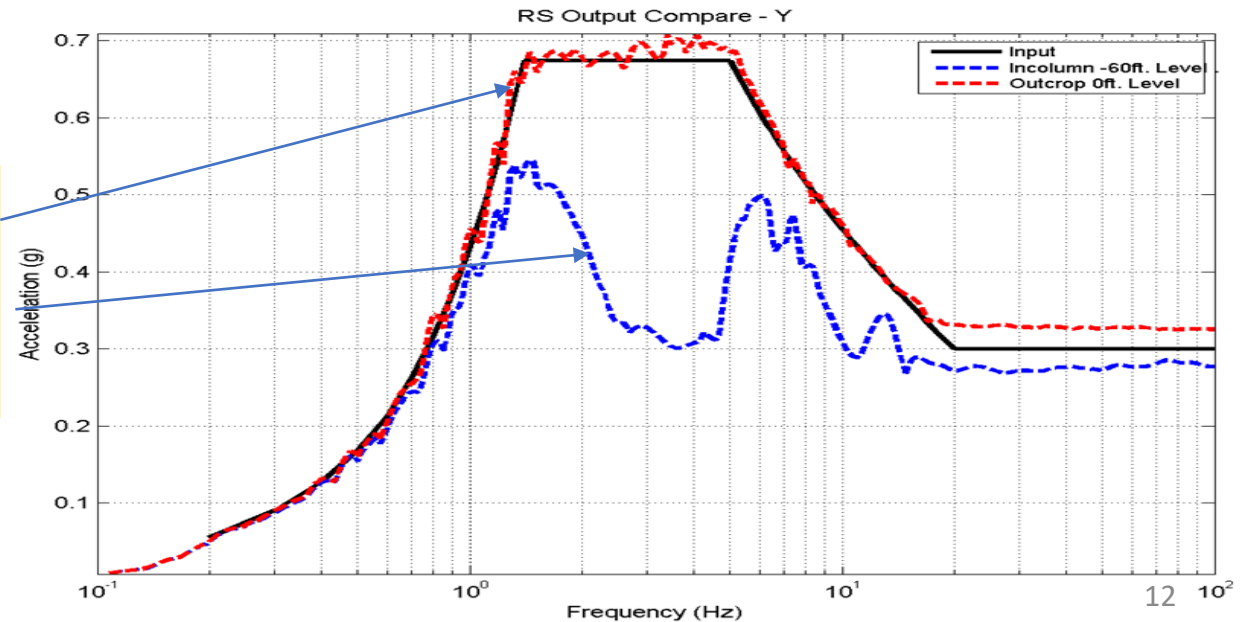
The octahedral shear strain from computed for each input direction X, Y and Z were combined before considering the nonlinear behaviour in time domain.

Seismic Input Motion and Soil Layering Cases

Soil Layering Cases

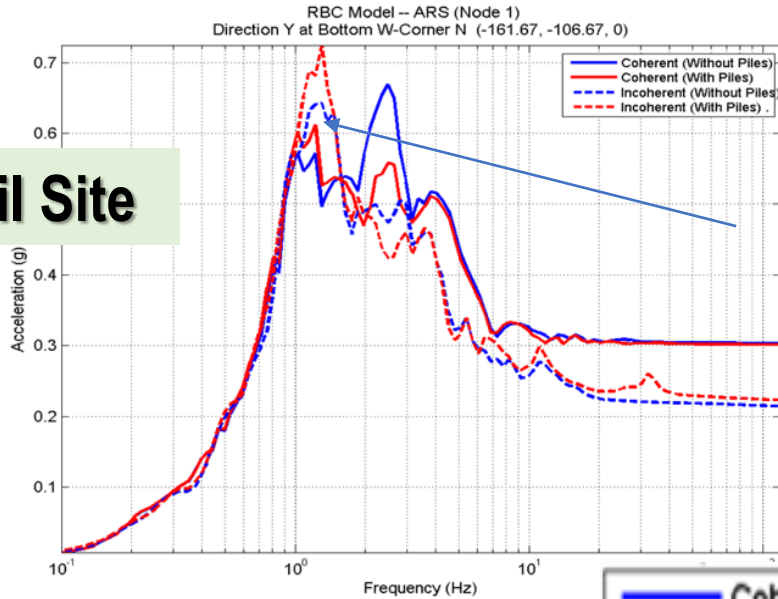


0.30g Eurocode DRS Seismic FIRS Input (Soil Site for IC)

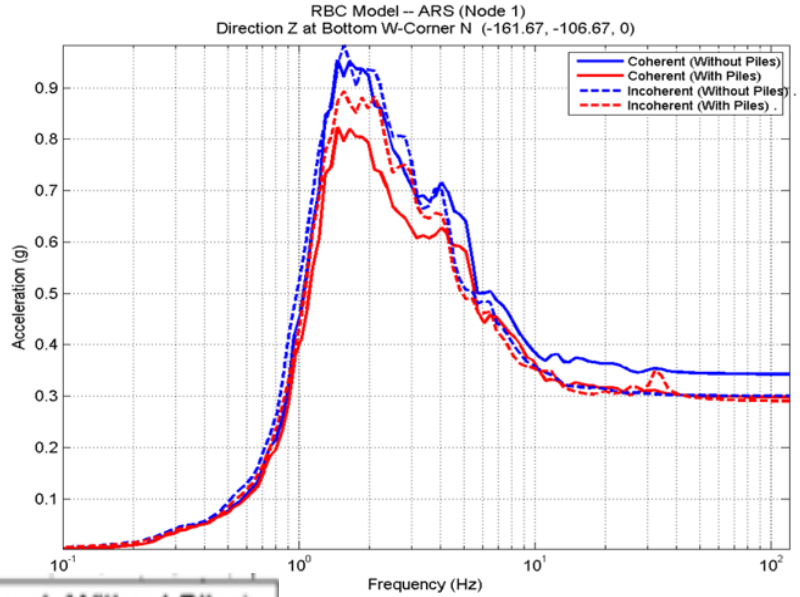


Basemat Corner ISRS *With* and *Without* Piles

Soil Site

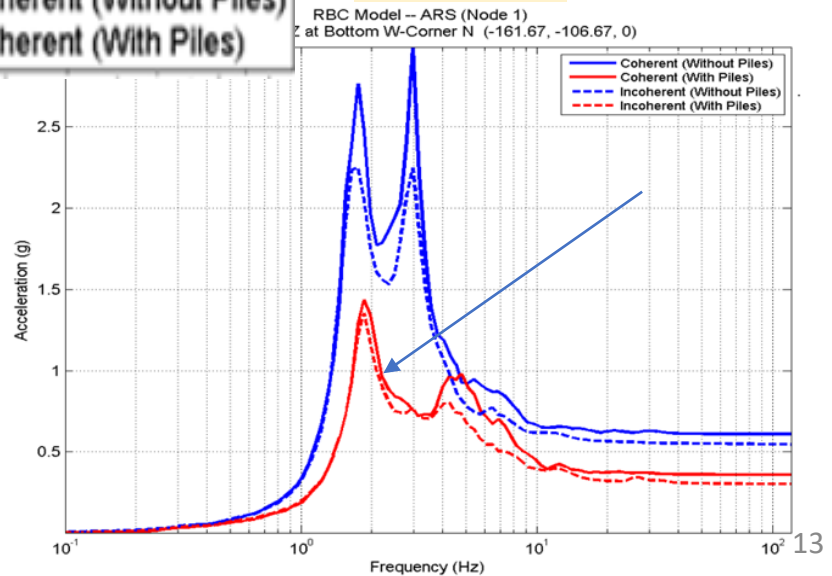
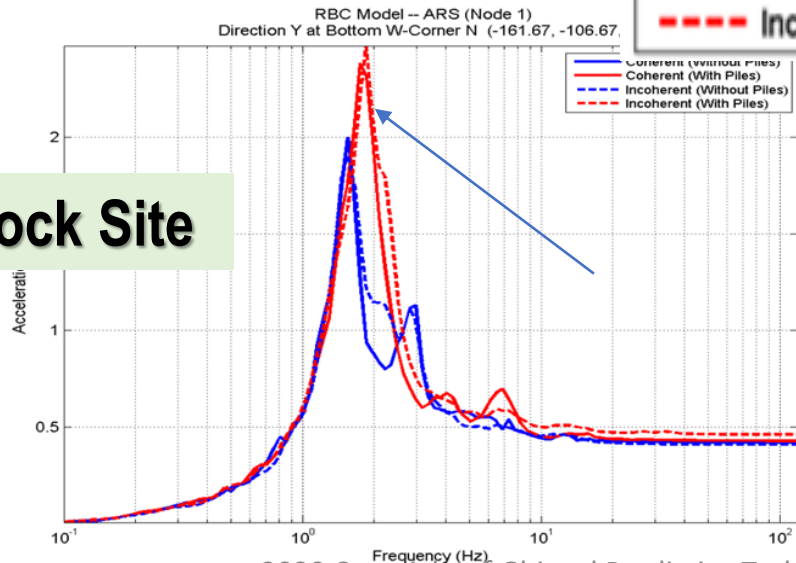


Horizontal



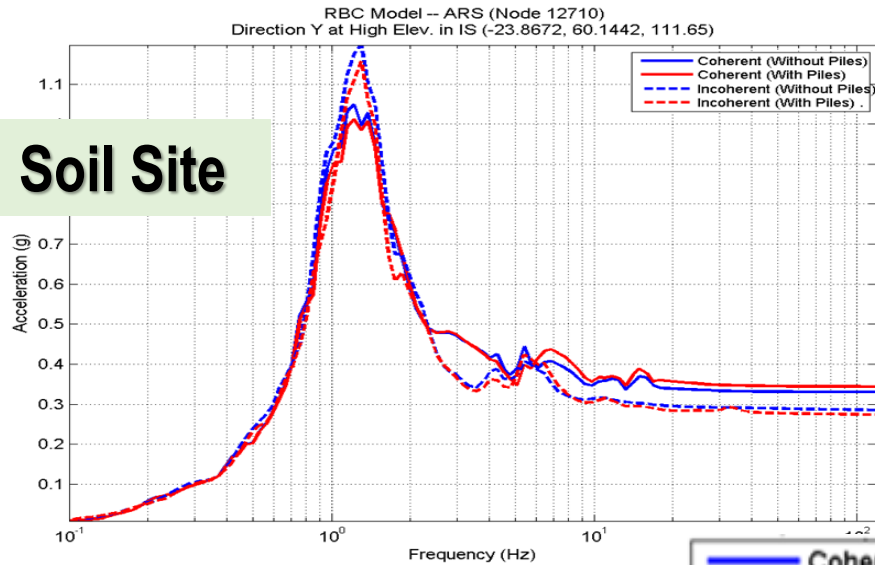
Vertical

Rock Site

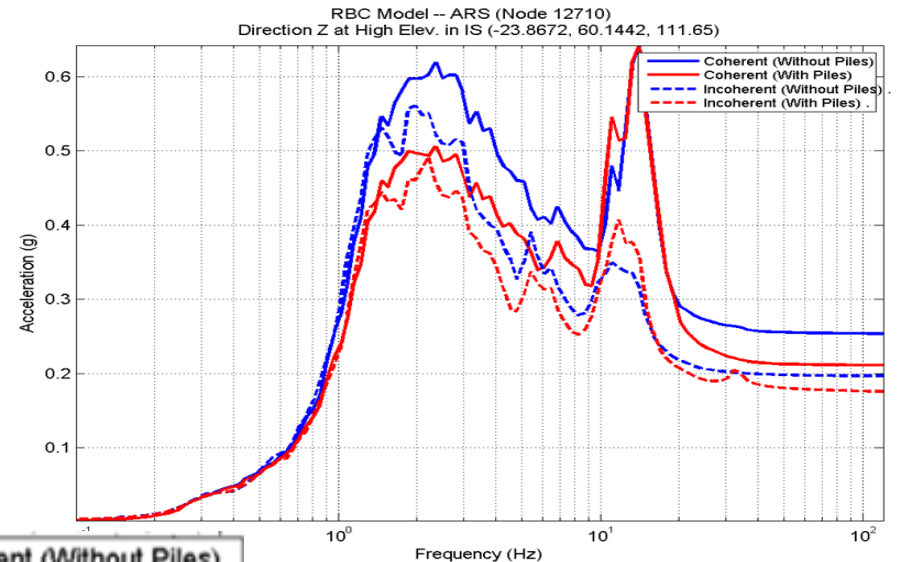


High-Elevation IS ISRS *With and Without Piles*

Soil Site

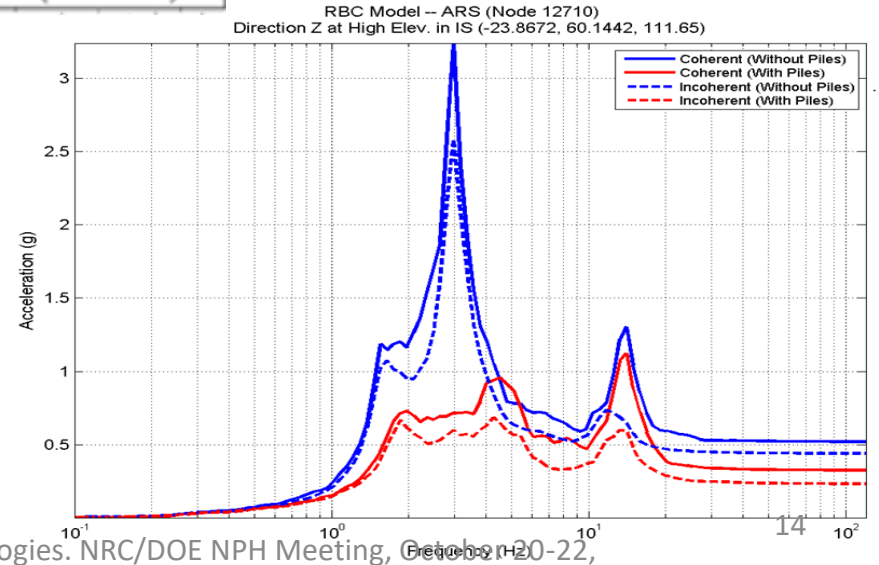
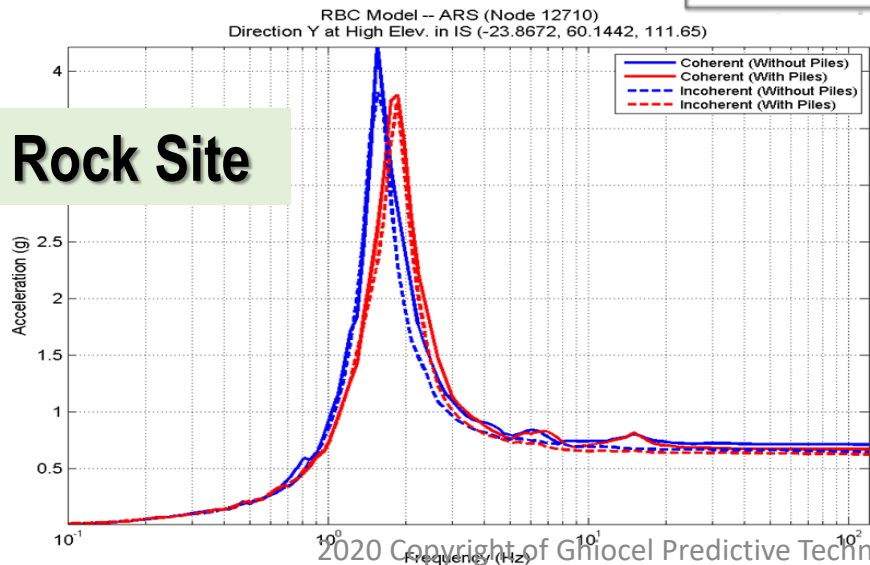


Horizontal



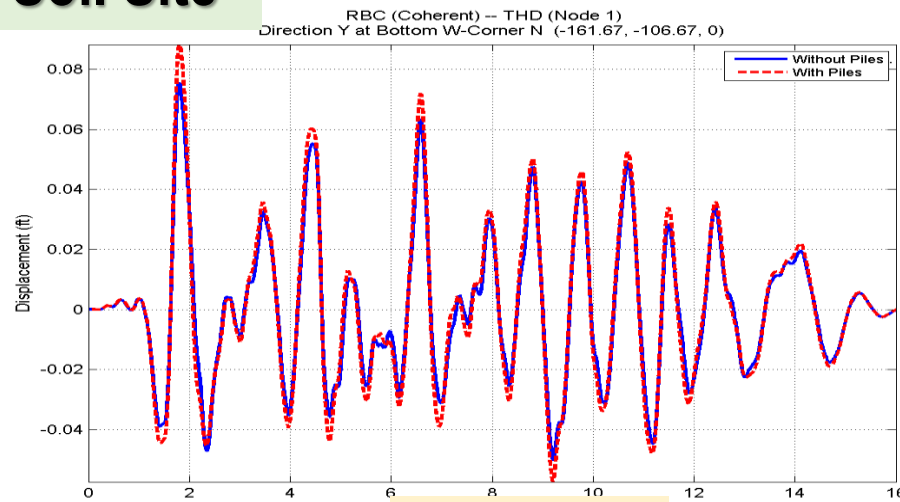
Vertical

Rock Site



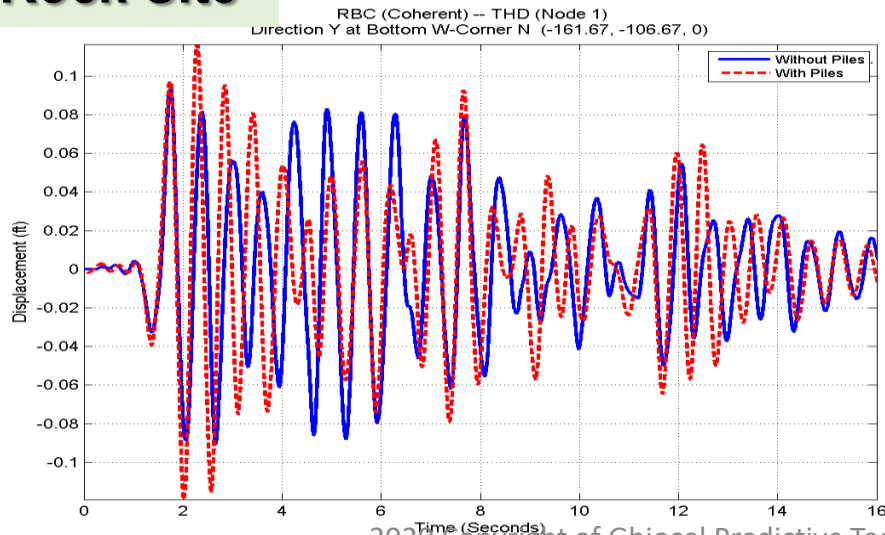
Basemat Corner Relative Displacements wrt Ground Surface *With* and *Without* Piles

Soil Site

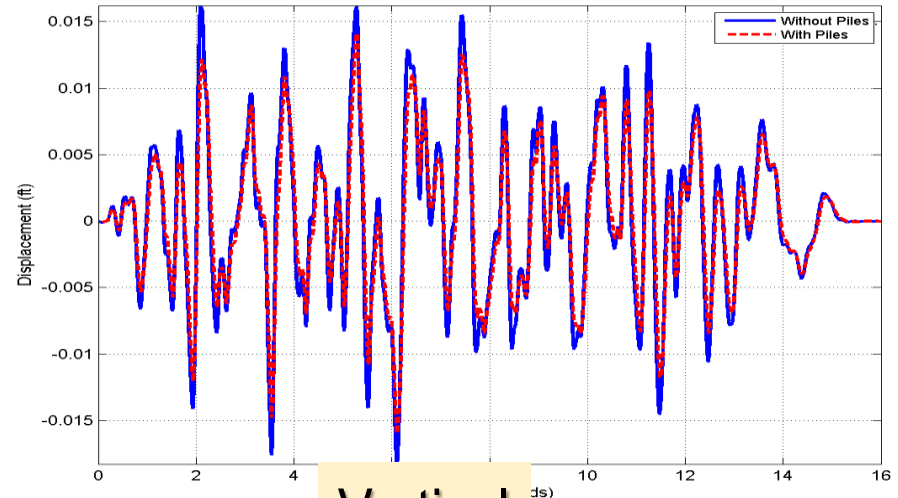


Horizontal

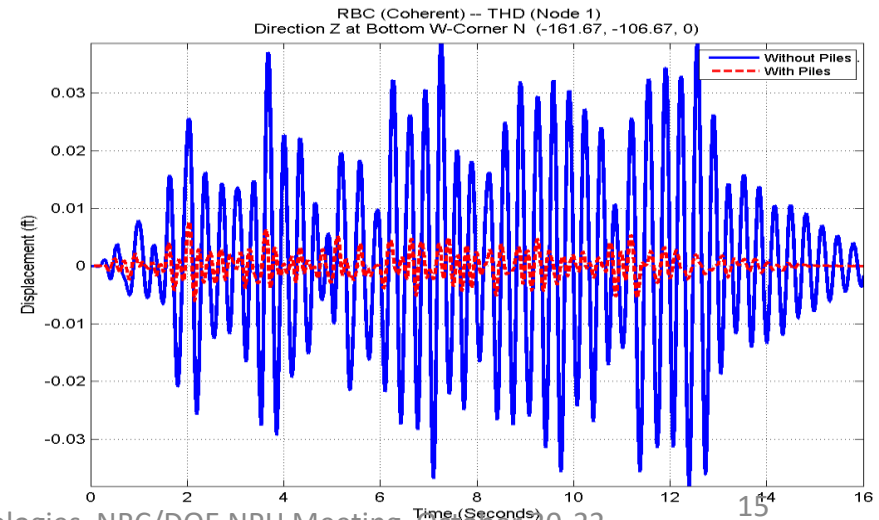
Rock Site



RBC (Coherent) -- THD (Node 1)
Direction Z at Bottom W-Corner N (-161.67, -106.67, 0)

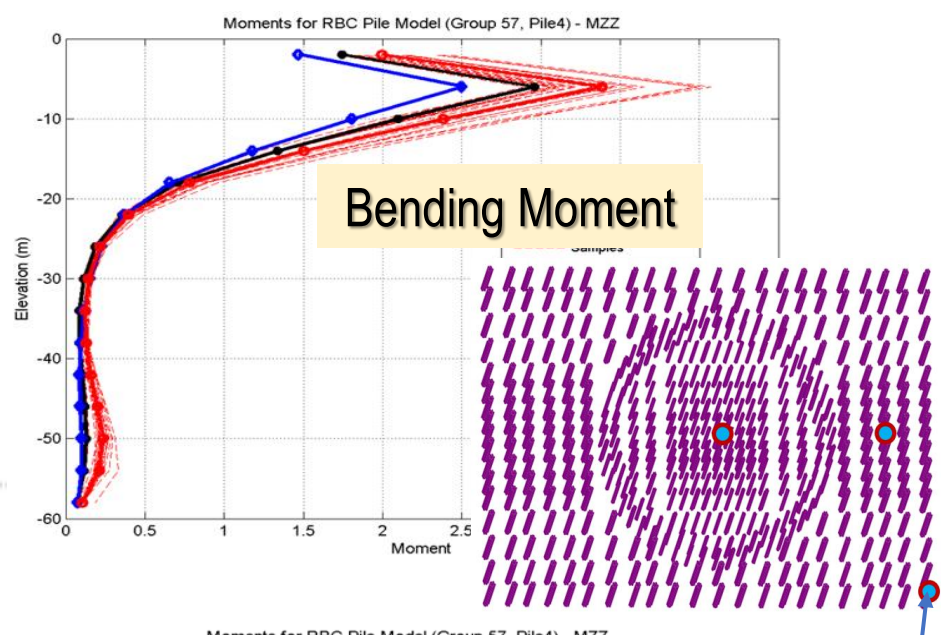
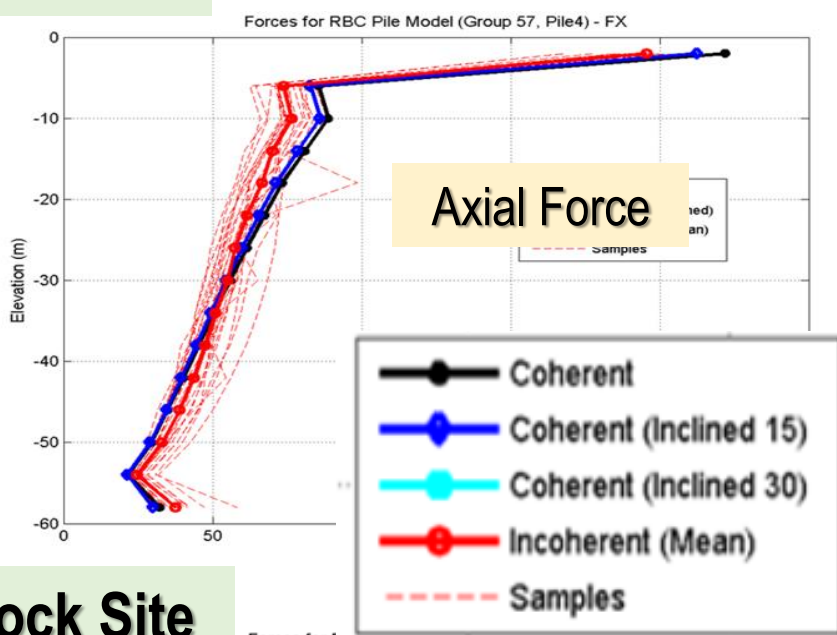


Vertical

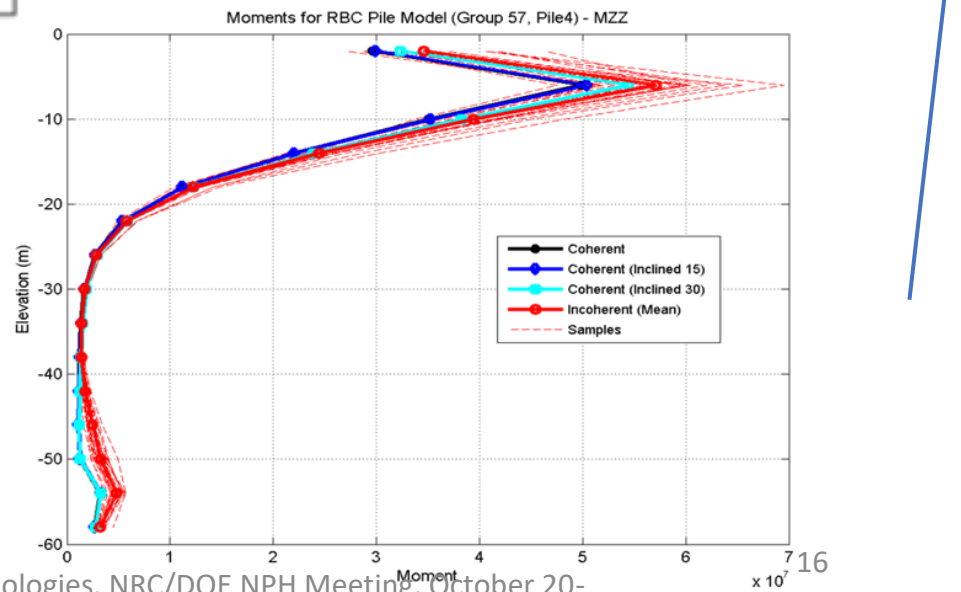
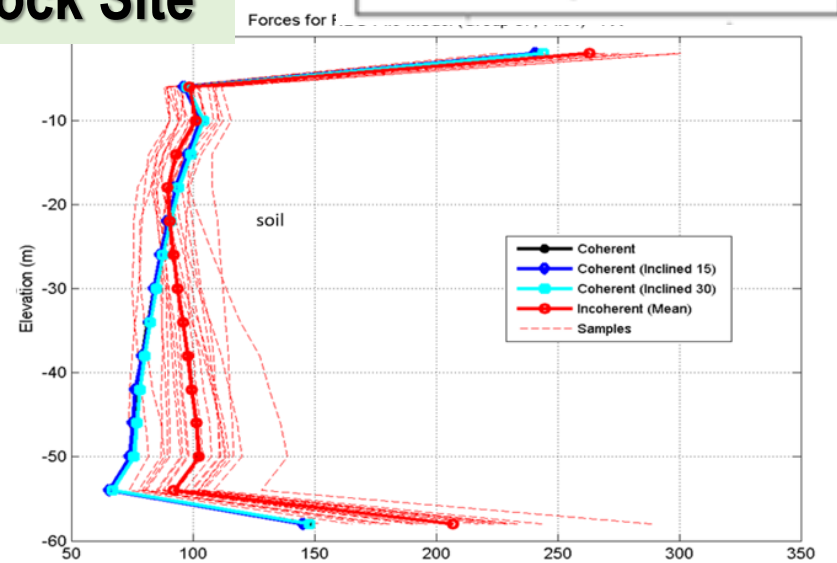


Axial Forces and Bending Moments in Corner Pile

Soil Site

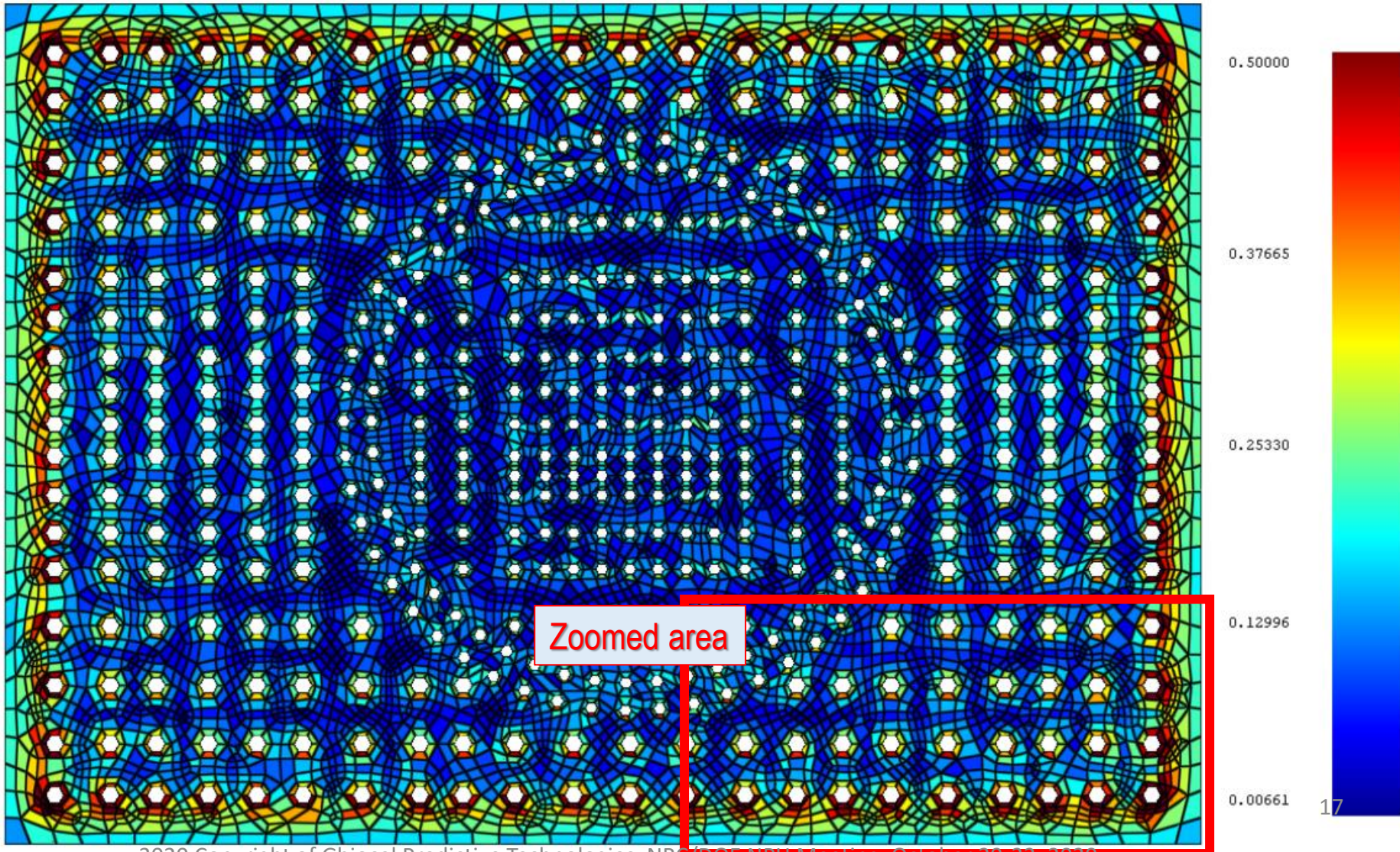


Rock Site



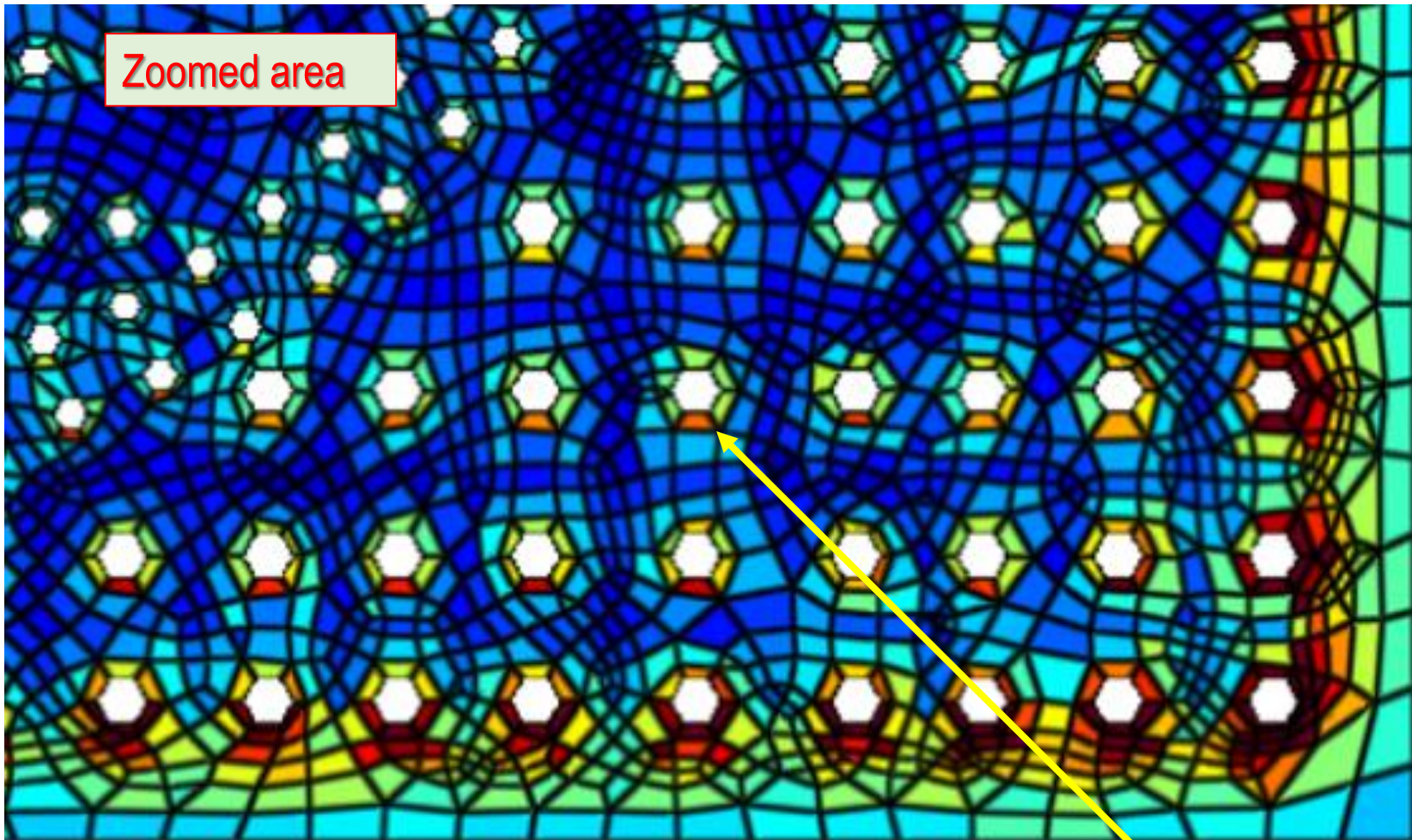
Nonlinear Soil Behavior in Vicinity of Piles

Effective (Iterated SSI) Soil Octahedral Shear Strain Under Combined X-Y-Z Seismic Inputs



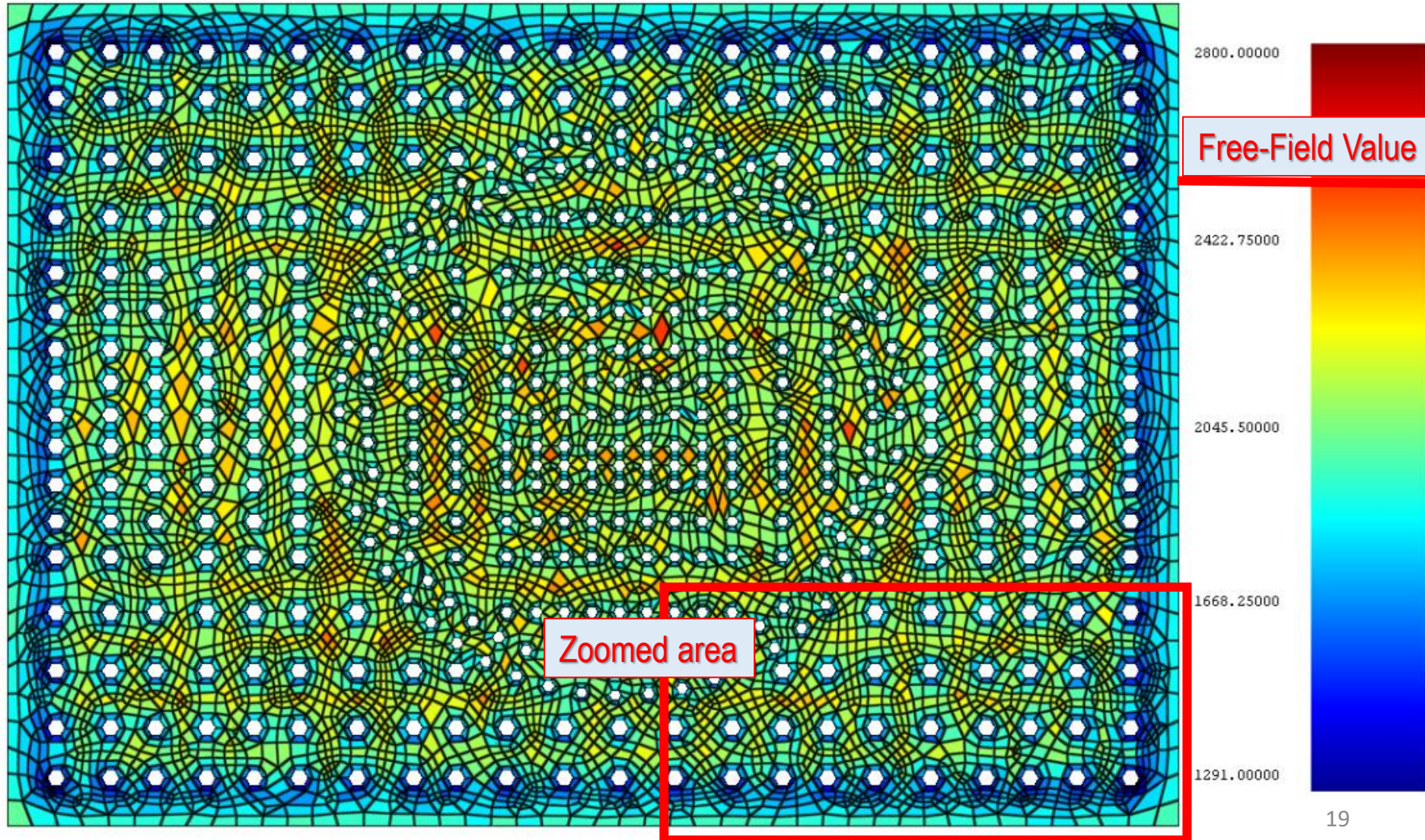
Nonlinear Soil Behavior in Vicinity of Piles

Effective (Iterated SSI) Soil Octahedral Shear Strain Under Combined X-Y-Z Seismic Inputs



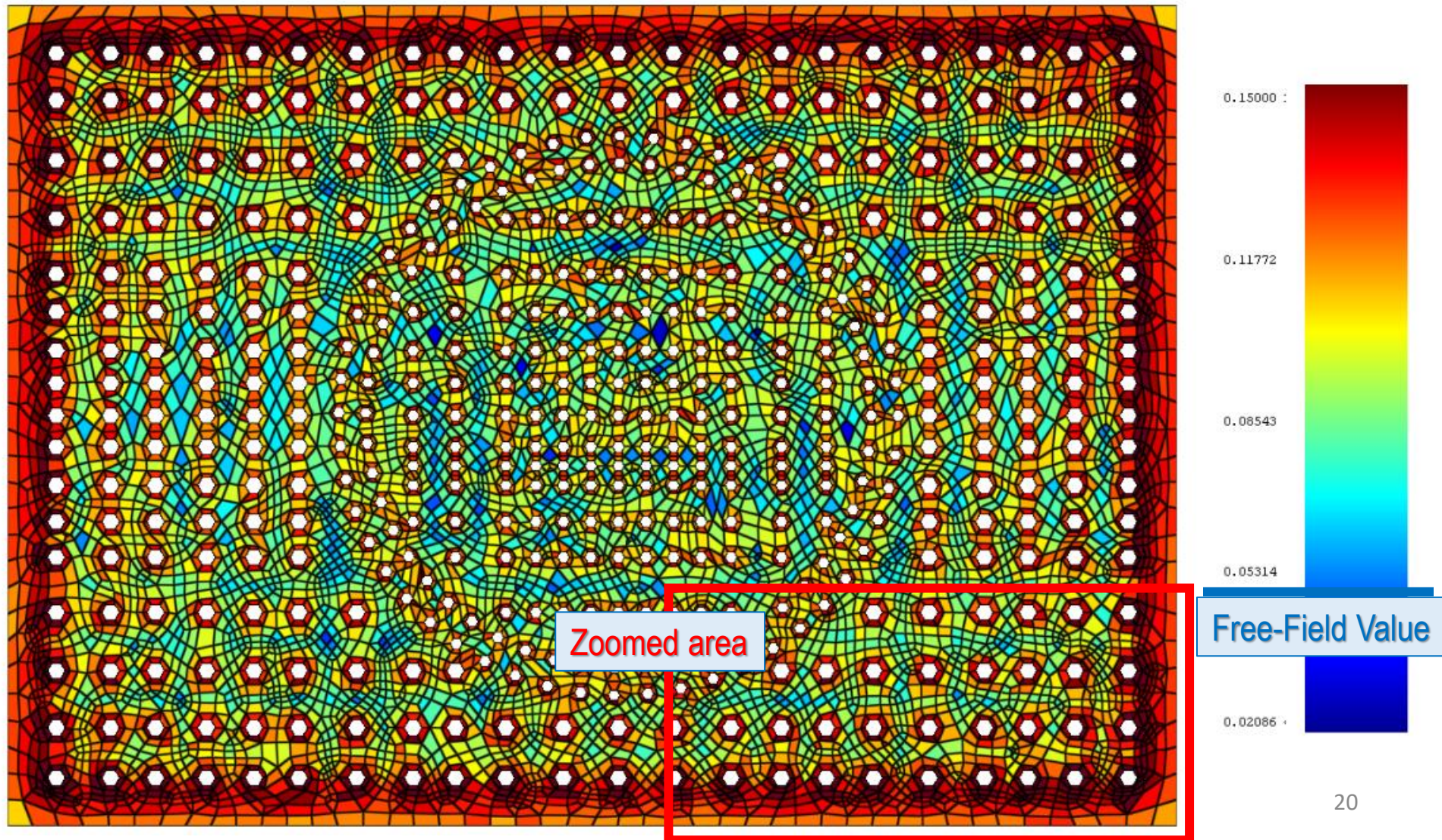
Nonlinear Soil Behavior in Vicinity of Piles

Effective (Iterated SSI) Soil Shear Modulus



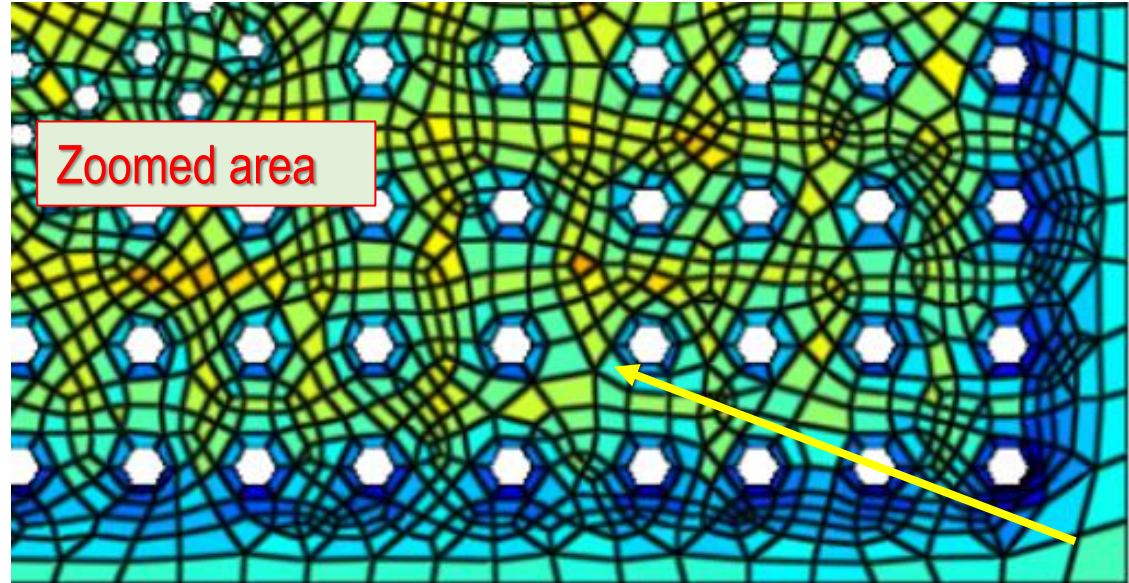
Nonlinear Soil Behavior in Vicinity of Piles

Effective (Iterated SSI) Soil Damping

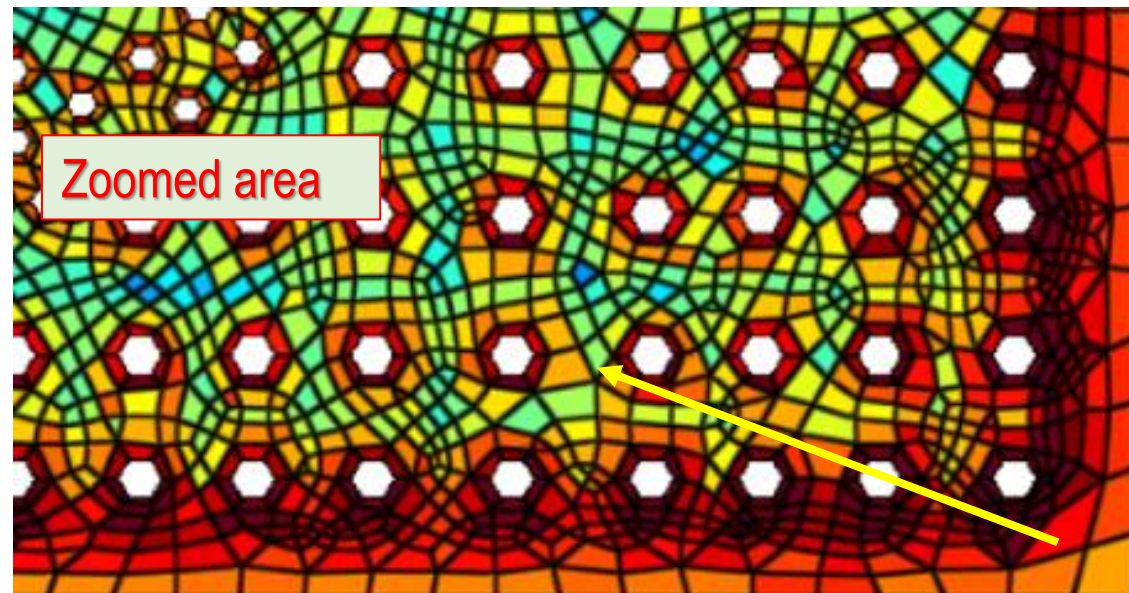


Nonlinear Soil Behavior in Vicinity of Piles

**Effective Soil
Shear Modulus**



**Effective Soil
Damping**

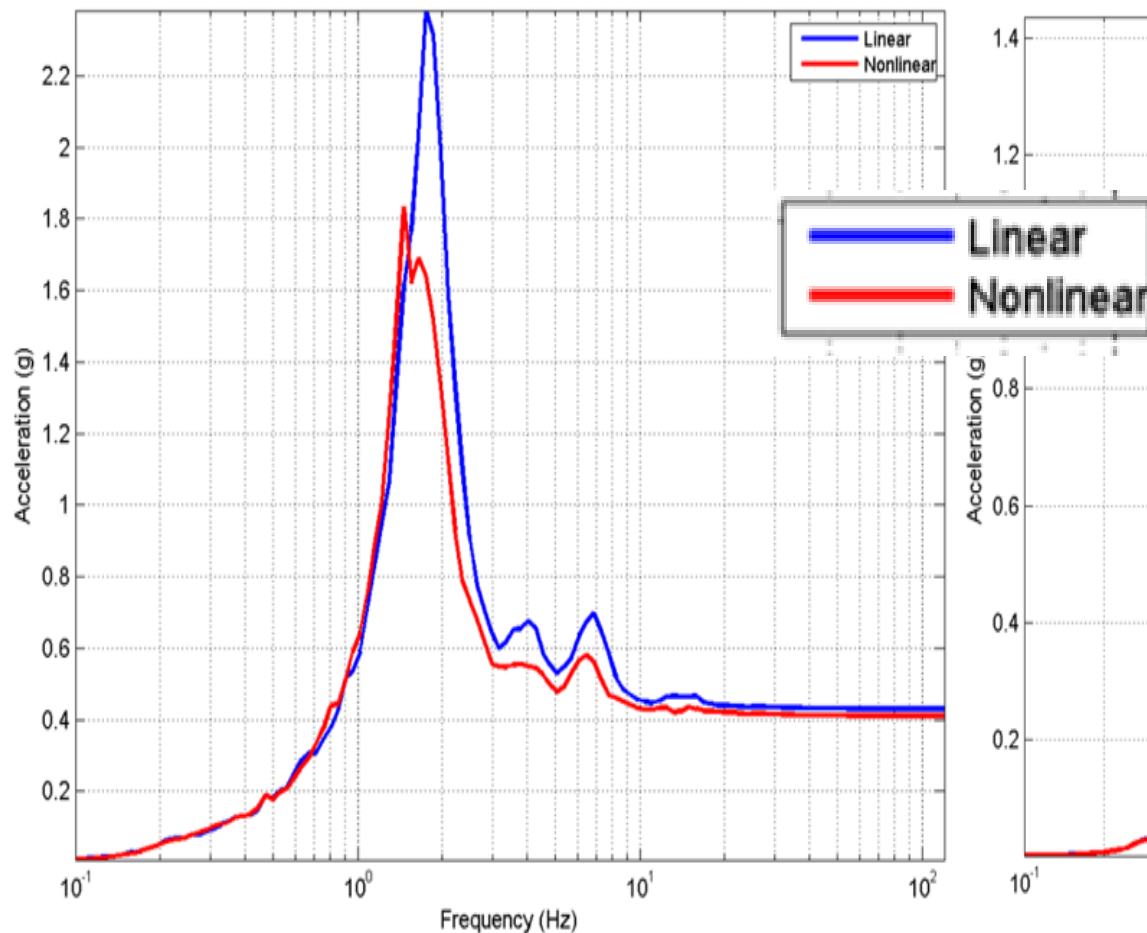


Nonlinear Soil Behavior in Vicinity of Piles.

ISRS at Basemat Level

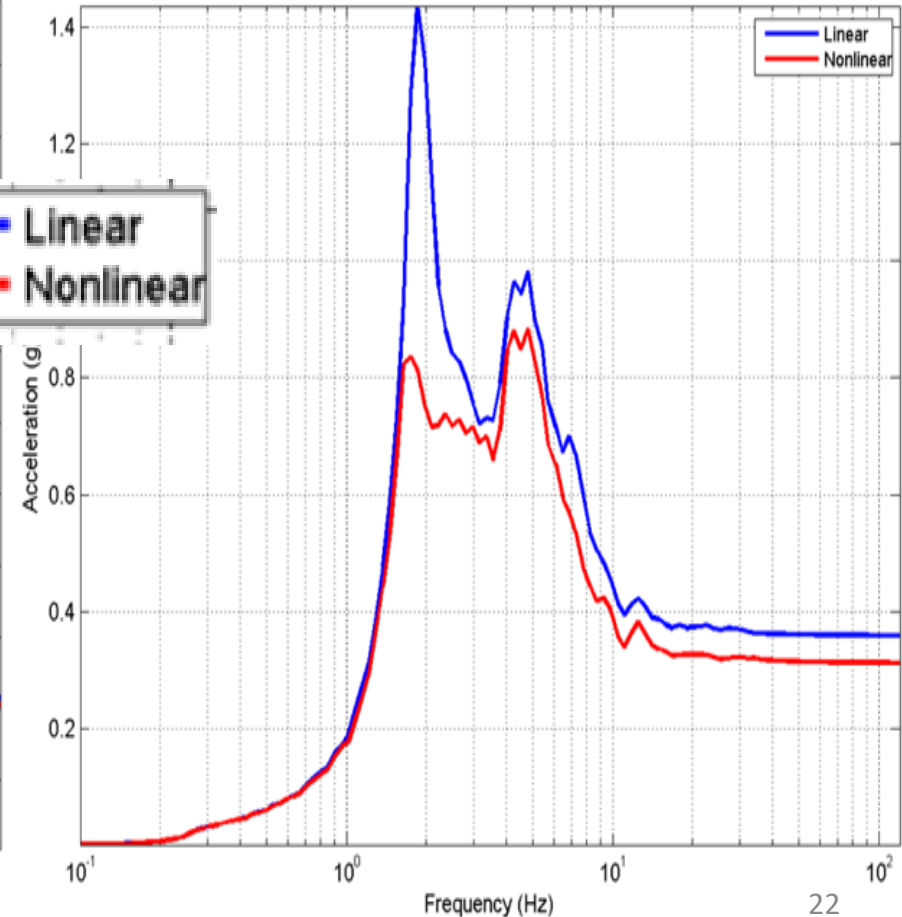
Horizontal

RBC Model (Coherent) -- ARS (Node 1)
Direction Y at Bottom W-Corner N (-161.67, -106.67, 0)



Vertical

RBC Model (Coherent) -- ARS (Node 1)
Direction Z at Bottom W-Corner N (-161.67, -106.67, 0)

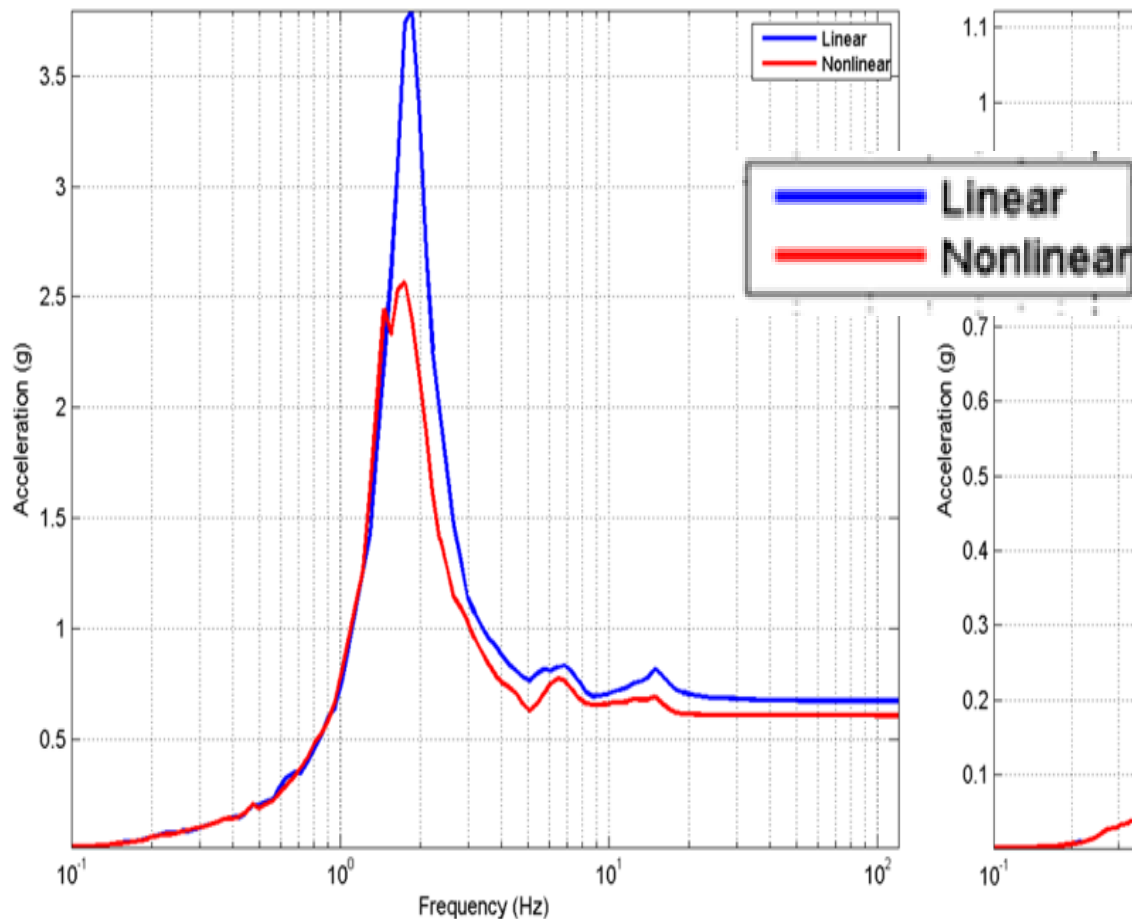


Nonlinear Soil Behavior in Vicinity of Piles.

ISRS at Top of IS

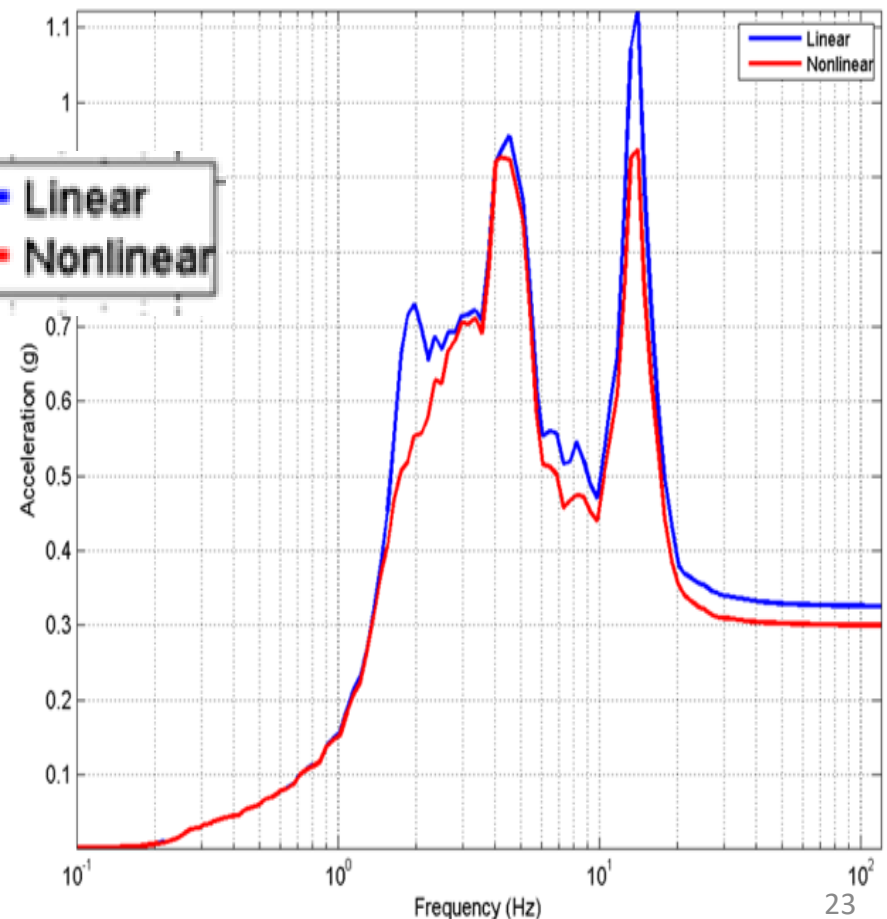
Horizontal

RBC Model (Coherent) -- ARS (Node 12710)
Direction Y at High Elev. in IS (-23.8672, 60.1442, 111.65)



Vertical

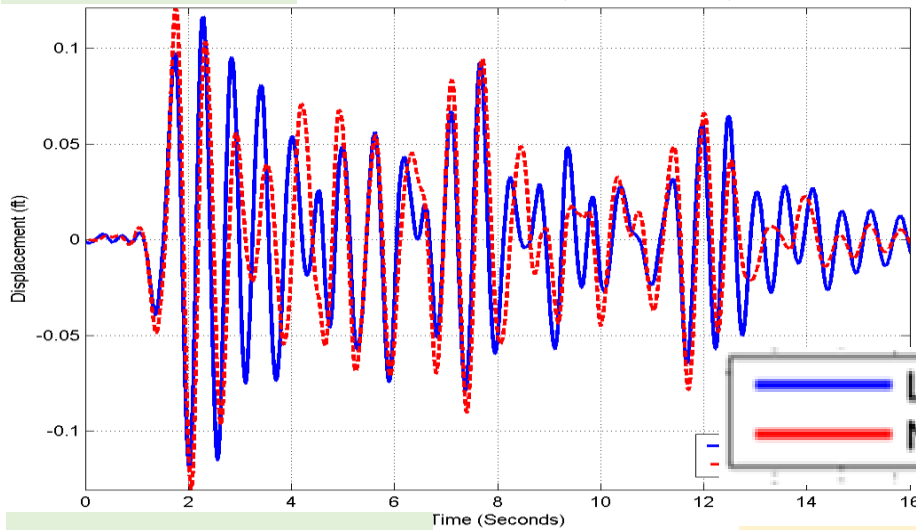
RBC Model (Coherent) -- ARS (Node 12710)
Direction Z at High Elev. in IS (-23.8672, 60.1442, 111.65)



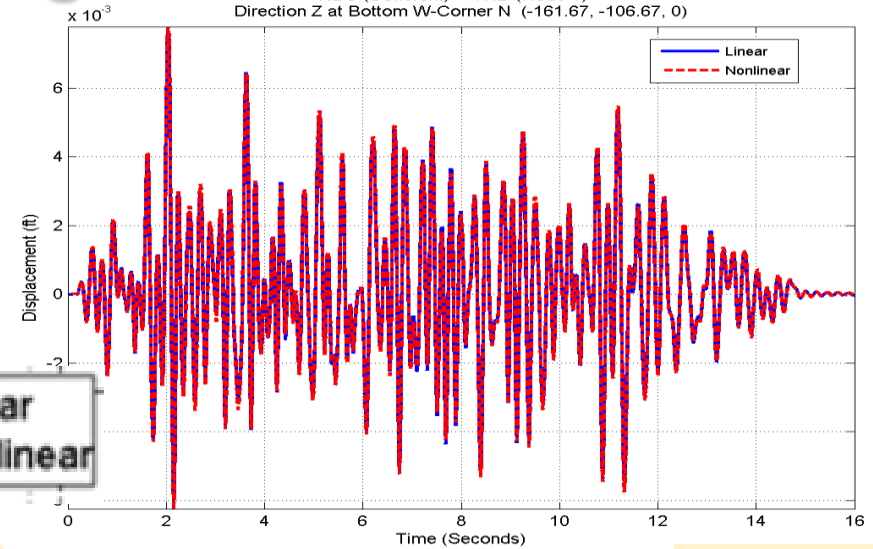
Displacements wrt Ground Surface at Basemat and High Elevation

Basemat

RBC (Coherent) -- THD (Node 1)
Direction Y at Bottom W-Corner N (-161.67, -106.67, 0)

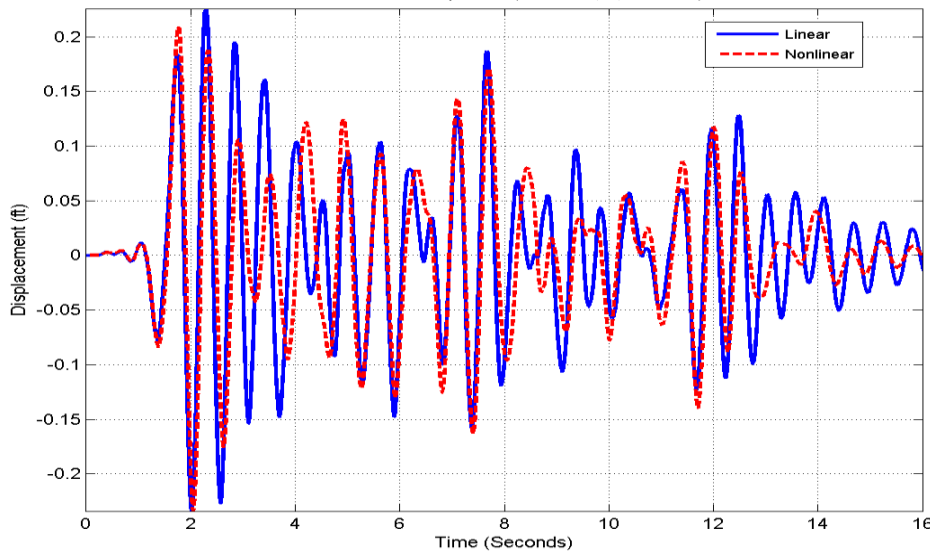


RBC (Coherent) -- THD (Node 1)
Direction Z at Bottom W-Corner N (-161.67, -106.67, 0)



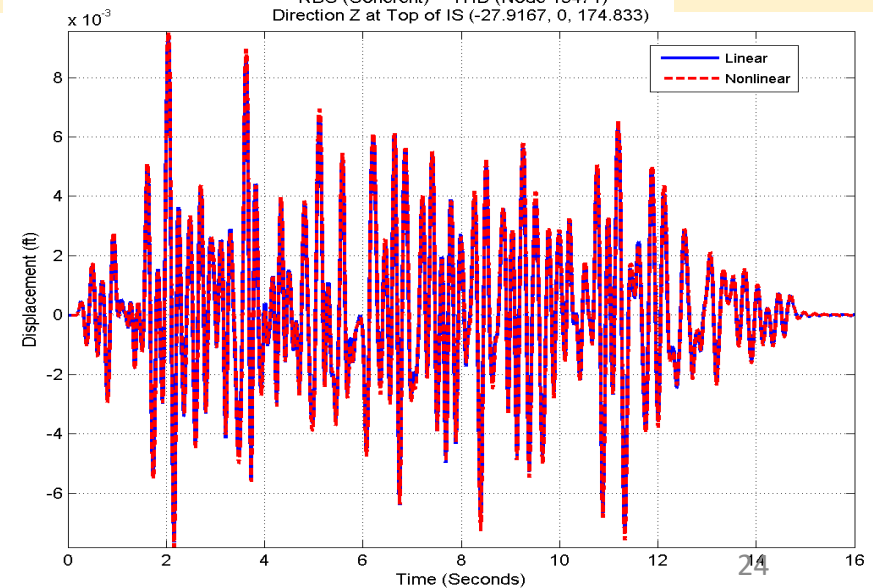
High Elevation

RBC (Coherent) -- THD (Node 15471)
Direction Y at Top of IS (-27.9167, 0, 174.833)



Horizontal

RBC (Coherent) -- THD (Node 15471)
Direction Z at Top of IS (-27.9167, 0, 174.833)



Vertical

3. Concluding Remarks

- The presentation describes an accurate and efficient SSI modelling for the pile foundation including the nonlinear soil behavior .
- Computed results show that the pile influence on various SSI responses is weak for the floating piles, and much more significant for the peak-bearing piles.
- Motion incoherency effects are reduced. Incoherency may increase pile axial forces and bending moments in corner piles.
- The nonlinear hysteretic soil behaviour in the vicinity of the piles reduces significantly the ISRS spectral peaks due to the large increase of soil material damping in the vicinity of piles.

Thank you!