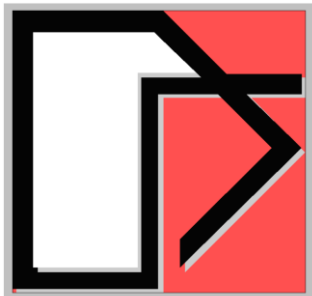


Probabilistic Seismic SSI Analysis Sensitivity Studies for Base-Isolated Nuclear Structures Subjected to Coherent and Incoherent Motions



Ghiocel Predictive Technologies Inc.

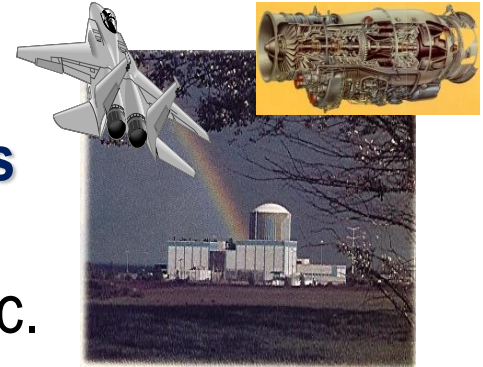
Dr. Dan M. Ghiocel

Member of ASCE 4 & 43 Standards

Email: dan.ghiocel@ghiocel-tech.com

Ghiocel Predictive Technologies Inc.

<http://www.ghiocel-tech.com>



**SMiRT25 Conference, Division III
Charlotte, NC, USA**

August 4-9, 2019

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Purpose of Presentation:

To investigate the effects of base isolation on seismic SSI response of a typical NI complex under coherent and incoherent motions using probabilistic and deterministic SSI analyses and different base-isolation systems, LRBs and HVDs.

The probabilistic and deterministic SSI analyses follow the recommendations of the ASCE 4-16 standard.

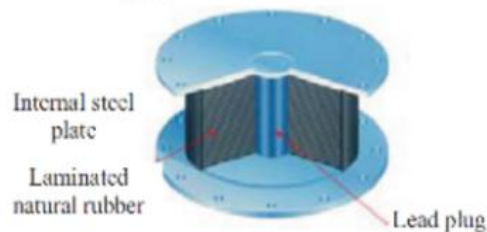
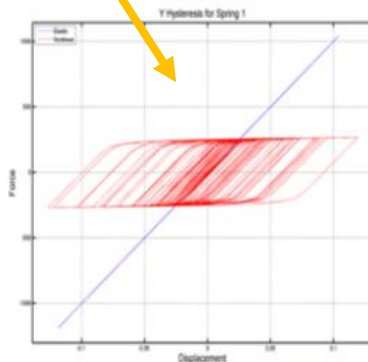
Sensitivity Studies

The presentation illustrate key results of a series of sensitivity studies, in two project phases, in 2015 (LRBs) and in 2019 (HVDs) to investigate

- 1) the effects of the base-isolation against no base-isolation for rock sites and soil sites,
- 2) the effects of motion incoherency on SSI responses
- 3) the use of probabilistic SSI vs. deterministic SSI analysis
- 4) the effects of using the 3D HVD base-isolators against the 2D LRB base-isolators.

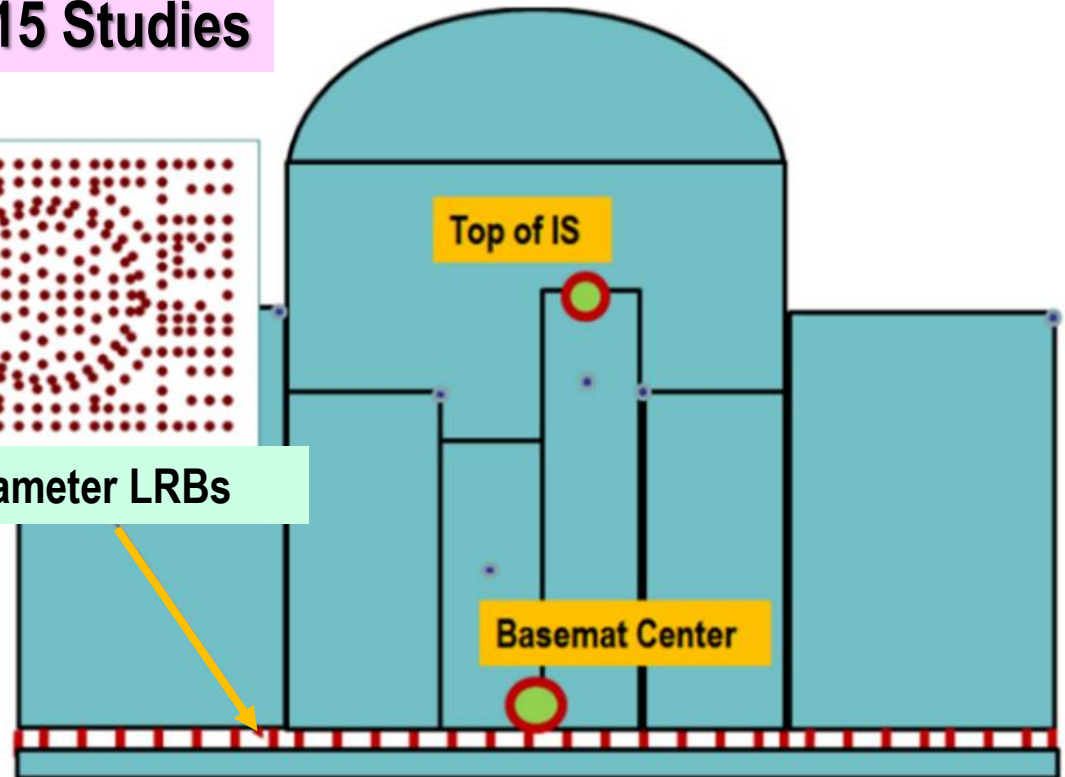
1. Effects of Seismic Base-Isolation on ISRS for Soil and Rock Sites and Coherent Motion

General Massing Rule
Hysteretic Model



2015 Studies

1.6m Diameter LRBs



Soil Layering:

SOIL: Uniform with $V_s = 1000$ fps

ROCK: Uniform with $V_s = 6000$ fps

Seismic Input:

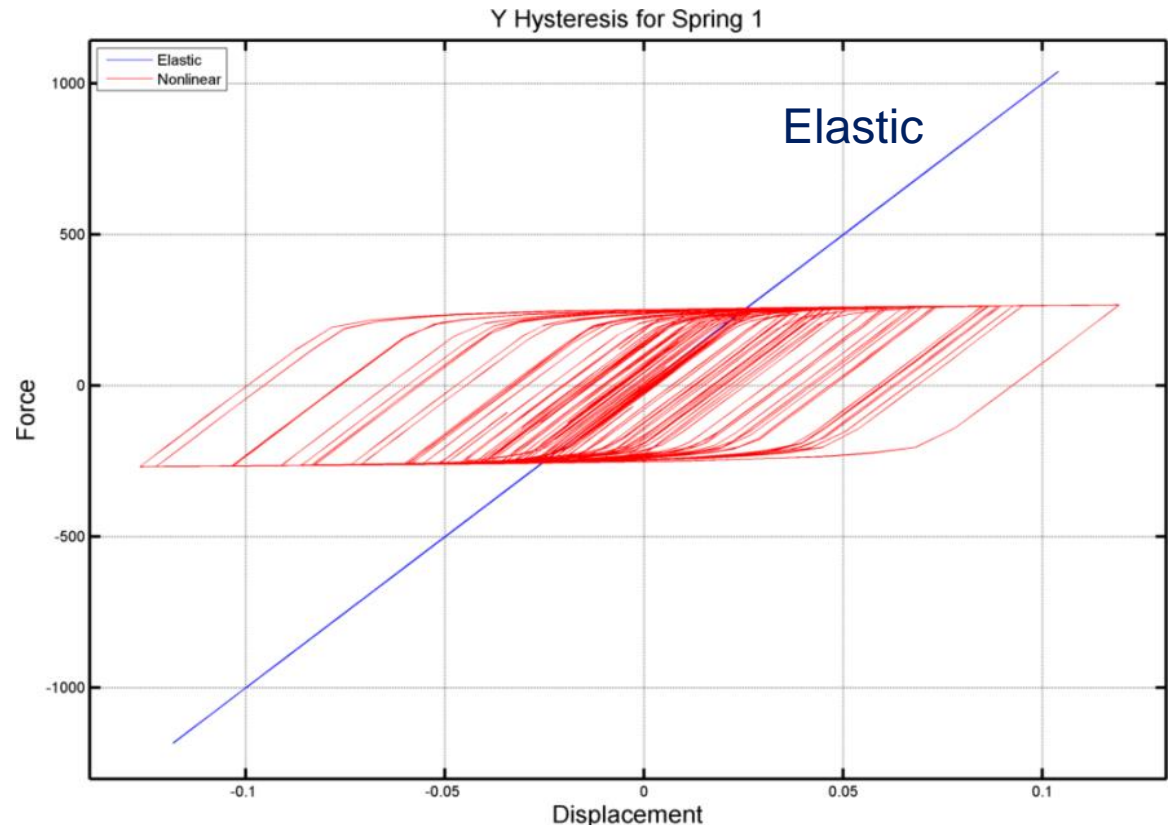
RG1.60 Input with 0.30g

Used ACS SASSI software with Option NON (nonlinear springs via iterative EQL SSI analysis)⁴

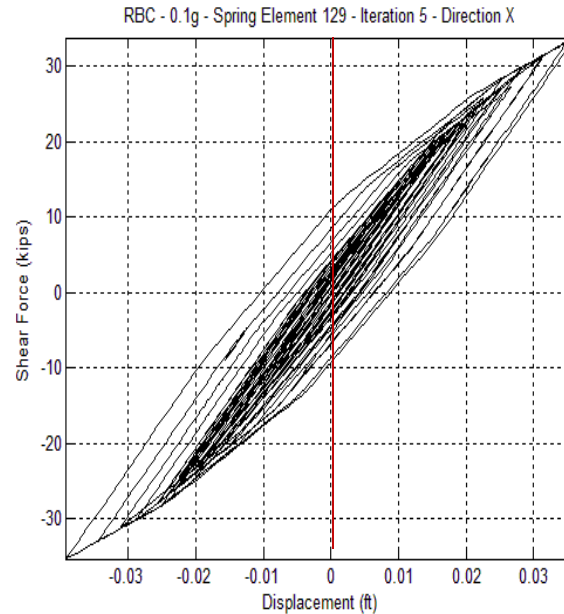
Modelling of the Hysteretic LRB Isolators

An efficient seismic SSI analysis was based on computing iteratively the SSI response for the equivalent-linearized system in complex frequency, coupled with an evaluation the local nonlinear spring behaviour in time domain for the simultaneous X, Y and Z inputs based on which the equivalent-linear spring is determined.

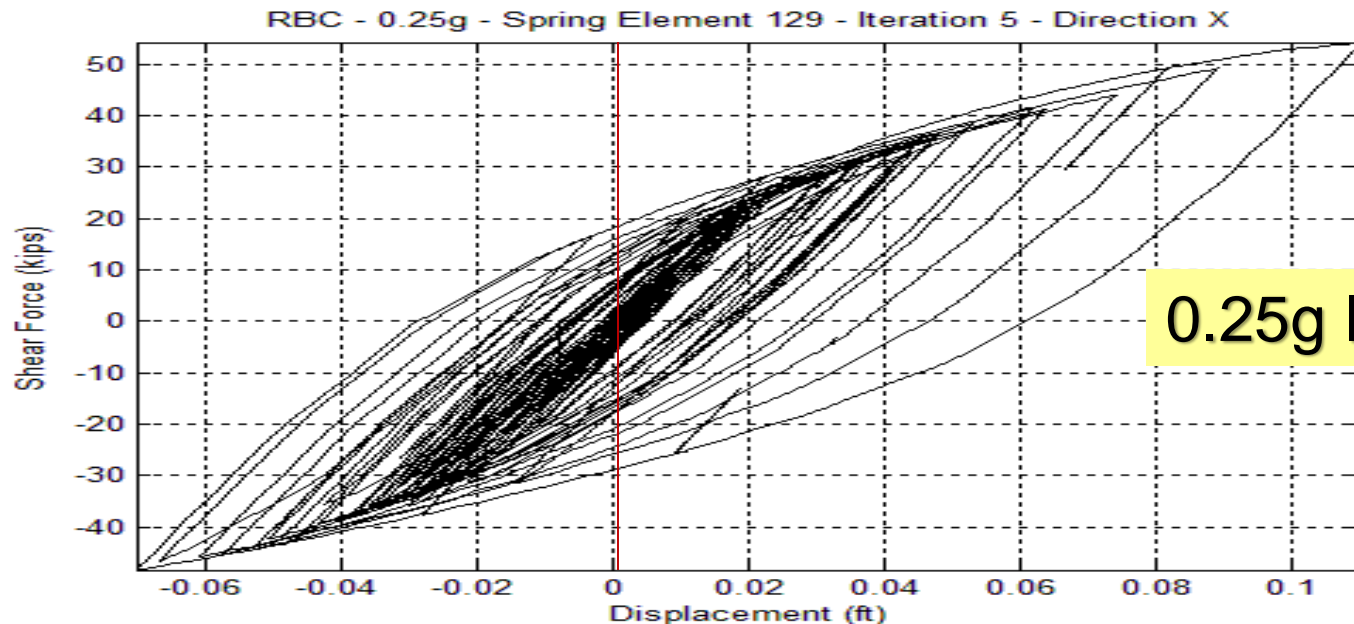
LRB Base-Isolator
Hysteresis Loop



General Hysteretic Model for LRB Isolators



0.10g Input

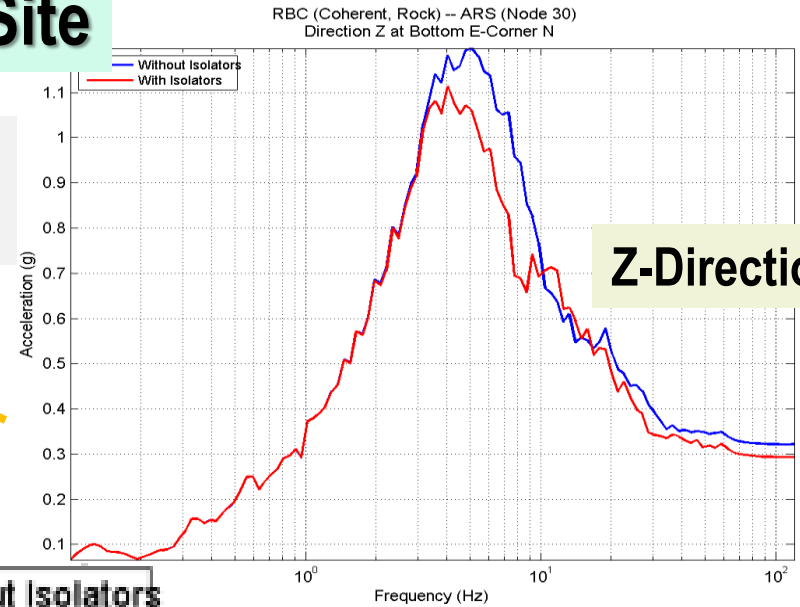
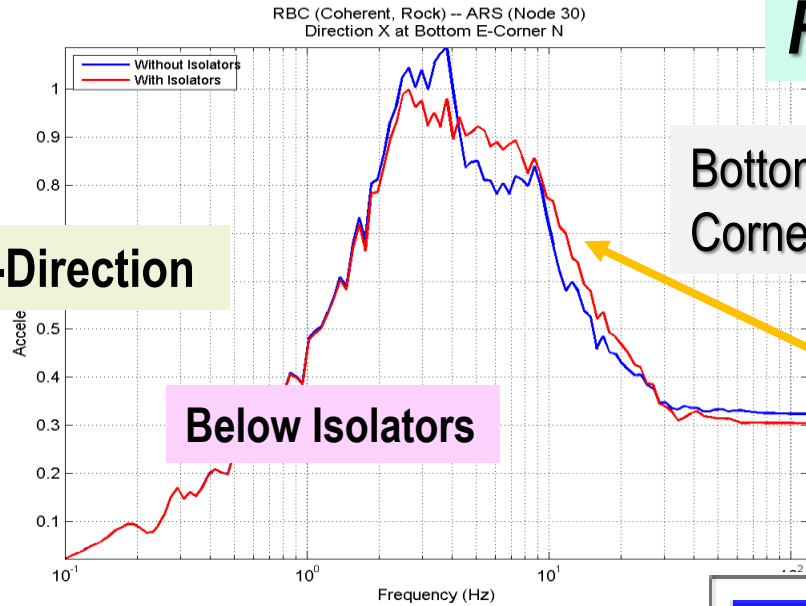


0.25g Input

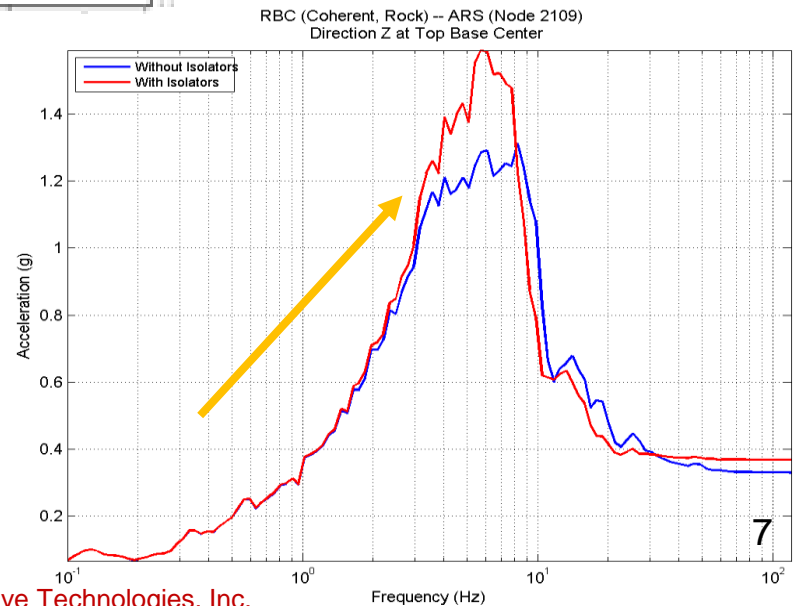
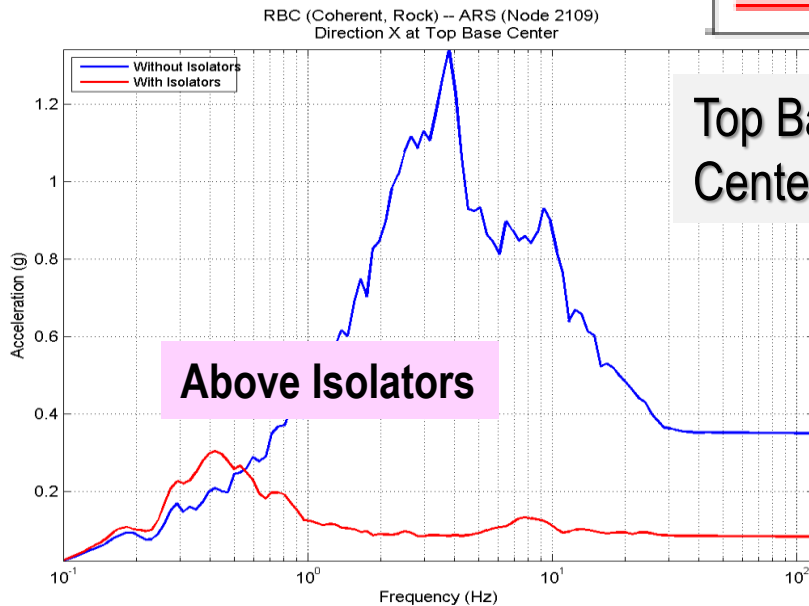
ISRS for NI Complex With and Without Isolators

Rock Site

X-Direction



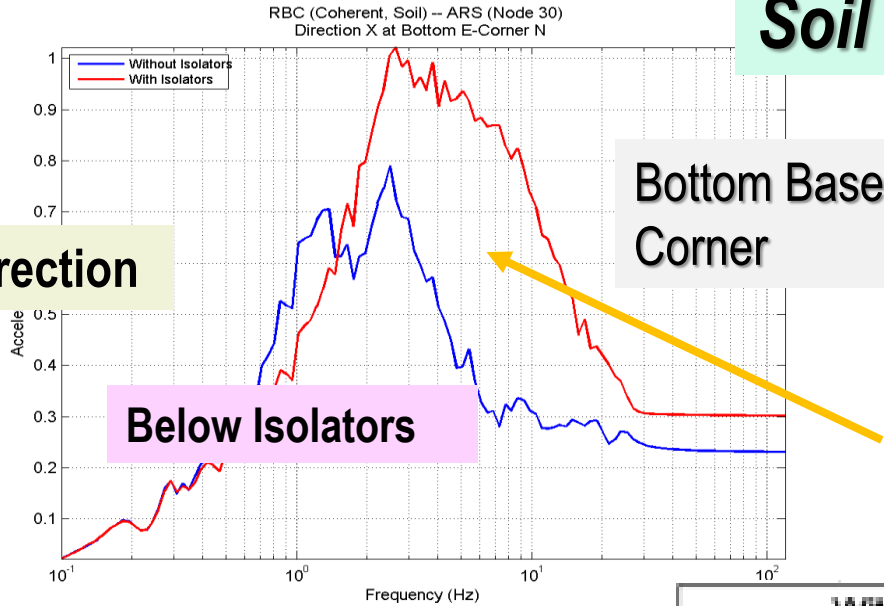
Top Base Center



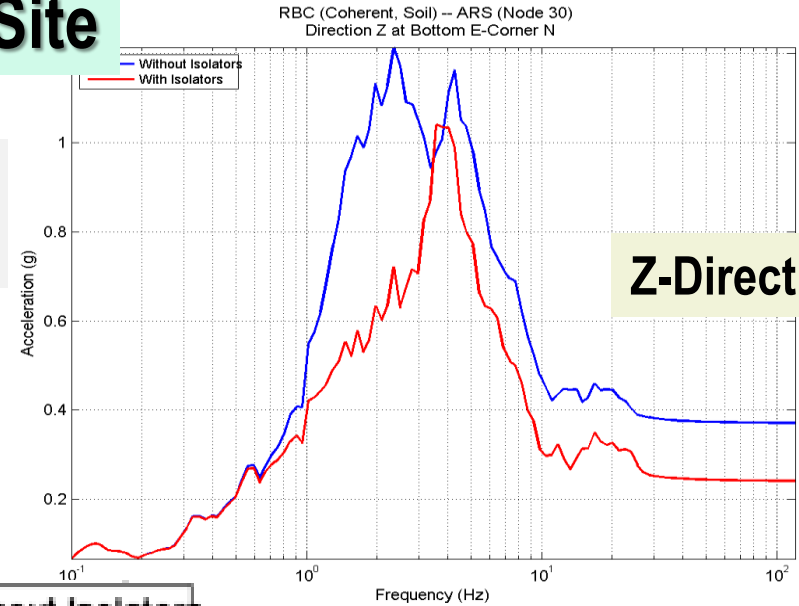
ISRS for NI Complex *With* and *Without* Isolators

Soil Site

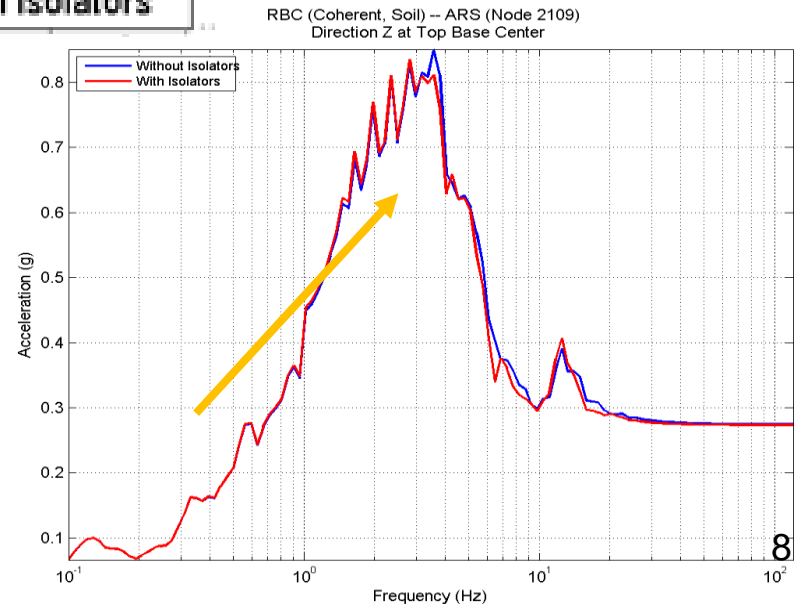
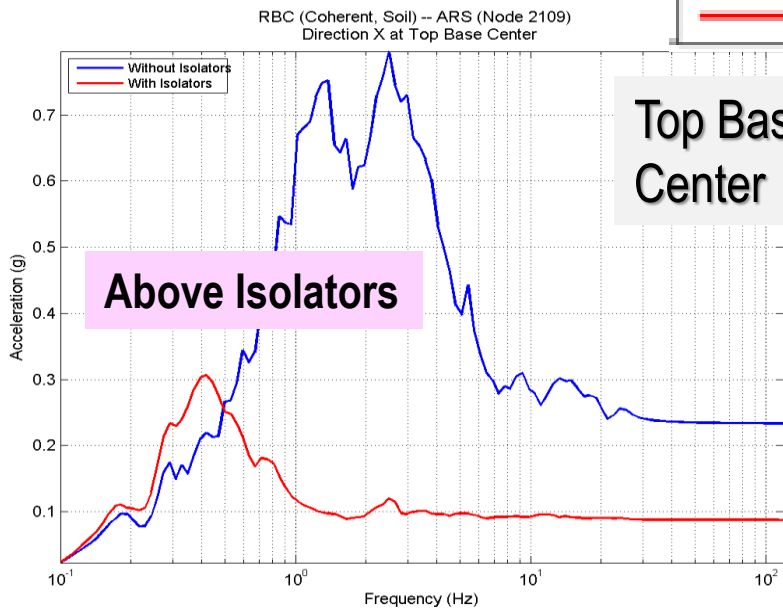
X-Direction



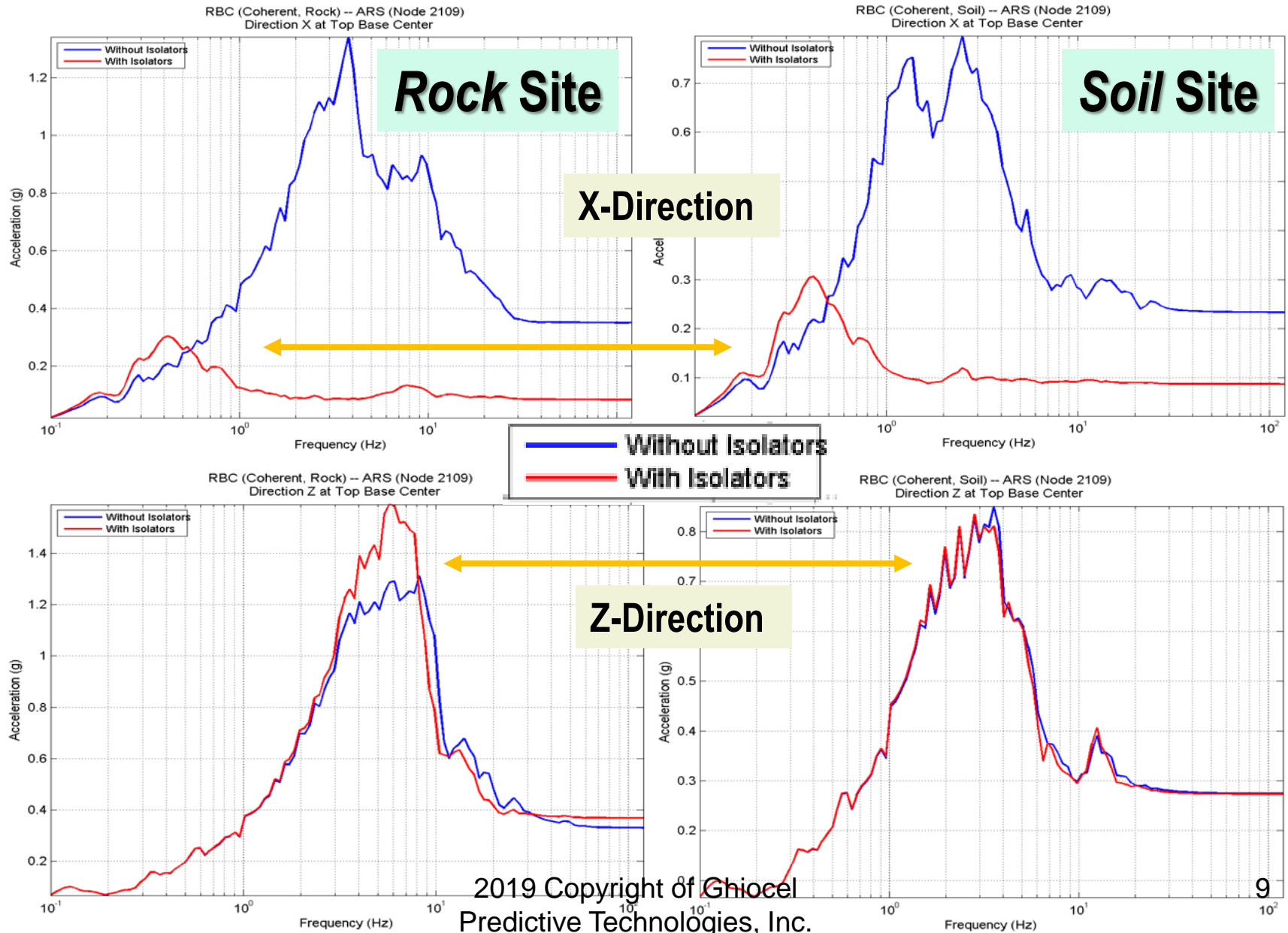
Z-Direction



Top Base Center

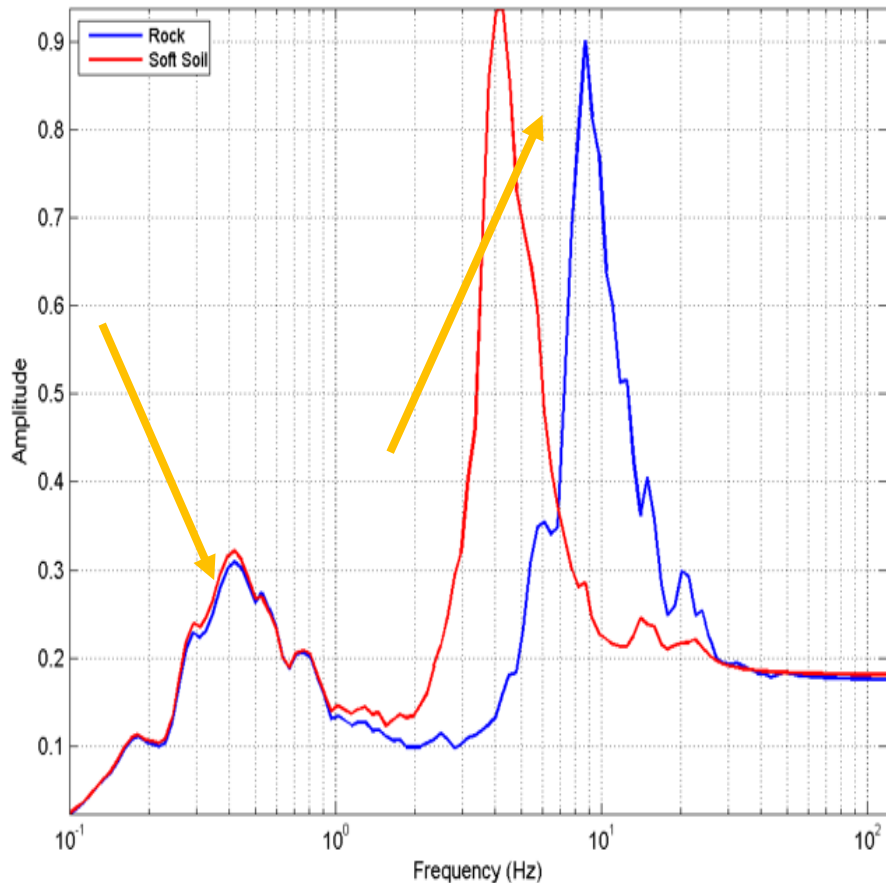


Top Basemat ISRS *With* and *Without* Isolators

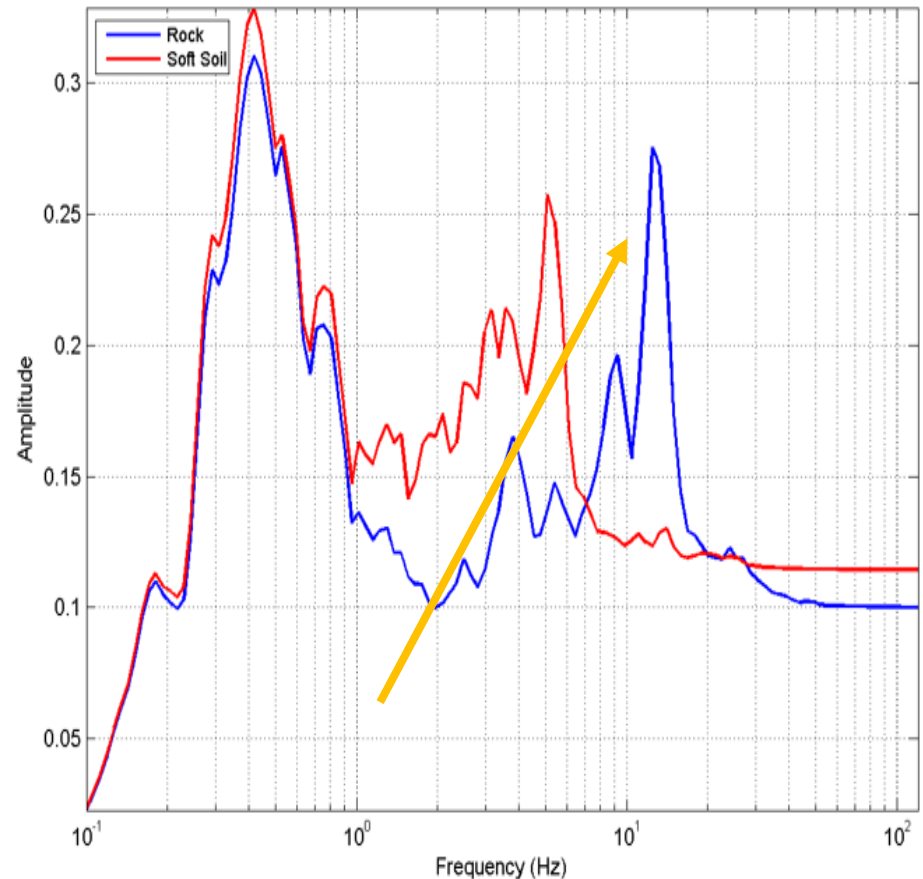


High-Elevation Horizontal ISRS *With Isolators* for Rock and Soil Sites

RBC (Col 8) **Location 1**



RBC (16391) **Location 2**



2. Effects of Motion Incoherency on ISRS

Incoherent Seismic Input:

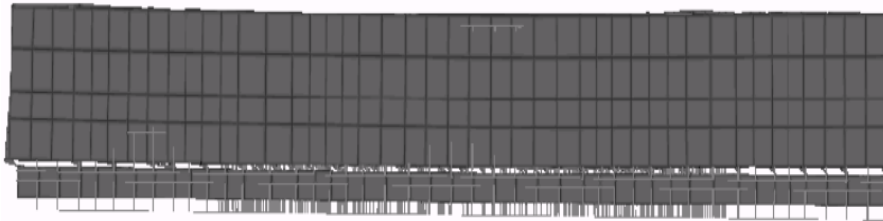
- For the comparative coherent vs. incoherent deterministic SSI analysis study, a uniform soil deposit with a V_s of 2,000 fps was considered.
- The incoherent motion was defined based on the Abrahamson coherence function for soil sites (Abrahamson, 2007).
- Additionally, an apparent traveling wave velocity of 6,000 fps was included to simulate the wave passage effects in the X-longitudinal direction.
- For the incoherent SSI analysis, the rigorous stochastic simulation approach (with no phase adjustment) based on a clean Monte Carlo wavefield simulations was used.
- Several incoherent seismic wavefields were simulated.

Coherent and Incoherent SSI Responses

Coherent Accelerations

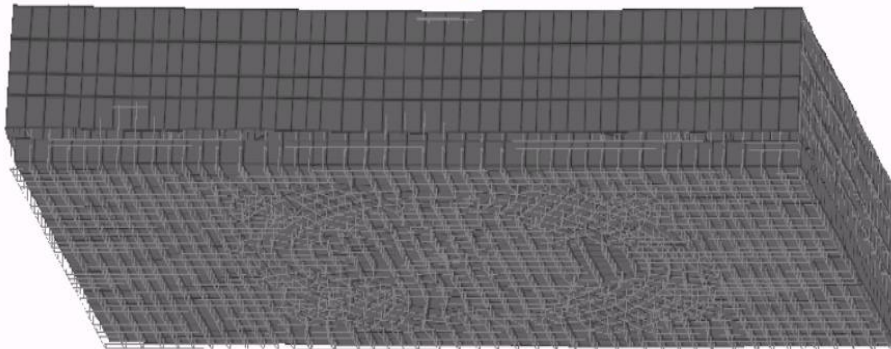
Rot: X = 90.000000 Y = -0.500000 Z = 0.000000
Zoom: 0.854998 Pen: X = -28.000000 Y = 177.000000
Screen Size: X = 874 Y = 630
Frame: 459

coherent



Rot: X = 105.000000 Y = -3.000000 Z = 10.000000
Zoom: 0.801999 Pen: X = -3.000000 Y = 176.000000
Screen Size: X = 874 Y = 630
Frame: 459

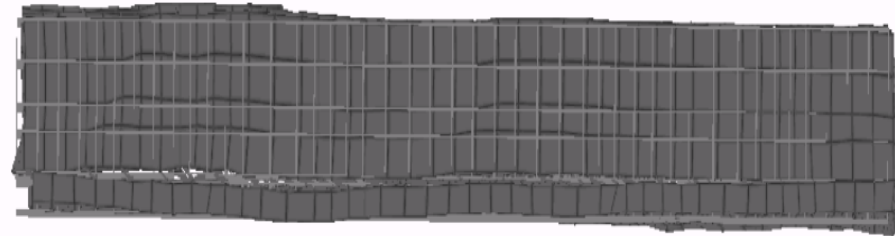
coherent



Incoherent Accelerations

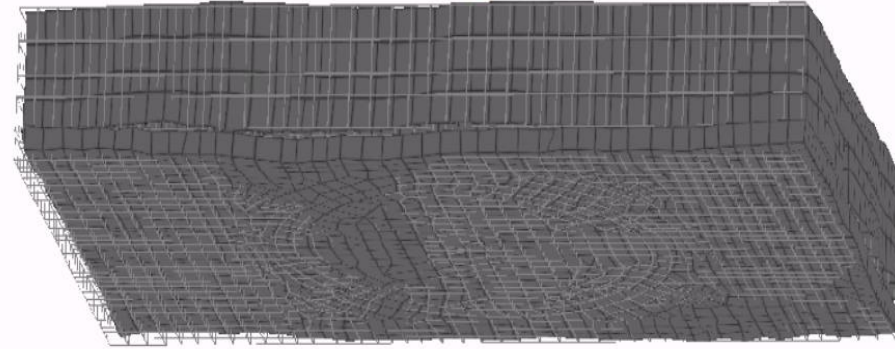
Rot: X = 90.500000 Y = -0.500000 Z = 0.000000
Zoom: 0.854999 Pen: X = 17.000000 Y = 184.000000
Screen Size: X = 874 Y = 630
Frame: 460

Incoherent 2



Rot: X = 105.500000 Y = -2.500000 Z = 10.000000
Zoom: 0.801000 Pen: X = 17.000000 Y = 184.000000
Screen Size: X = 874 Y = 630
Frame: 459

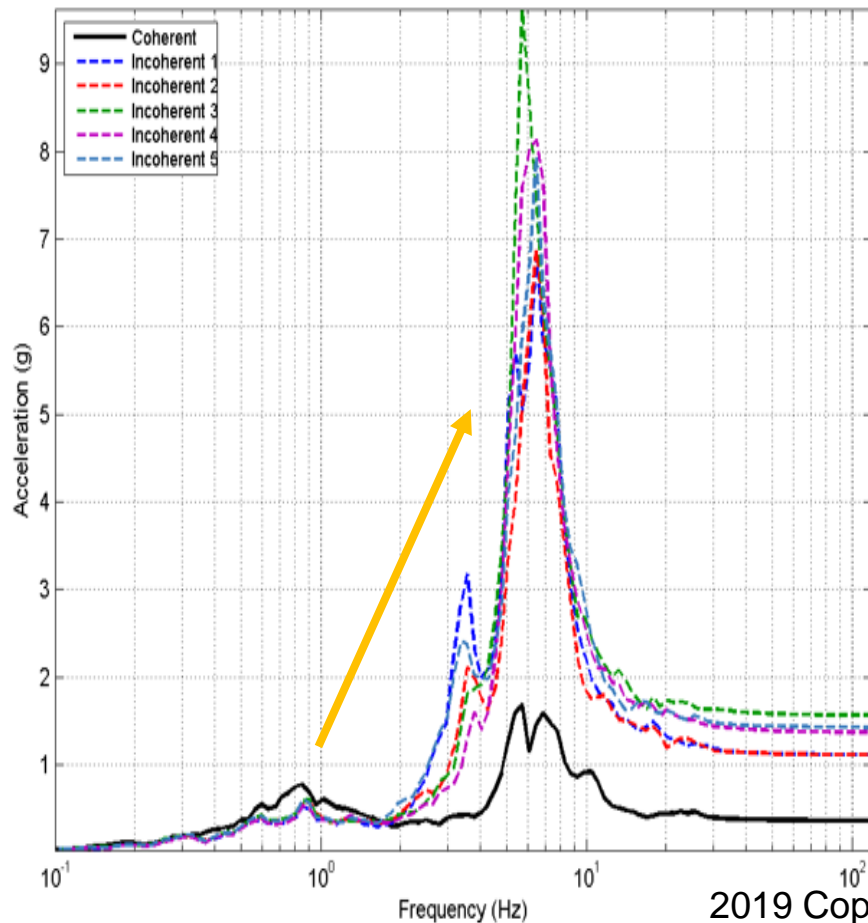
Incoherent 2



Horizontal and Vertical ISRS at Top of IS

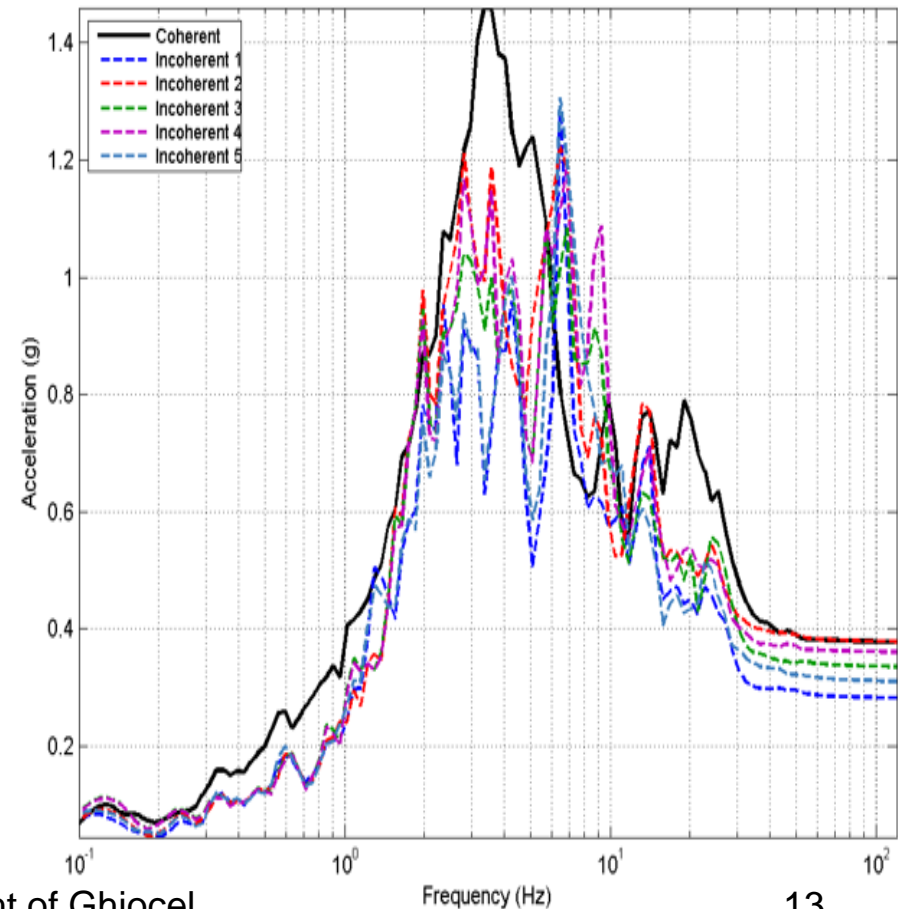
Horizontal

RBC (Medium Soil, With Isolators) – ARS (Node 15471)
Direction X at Top of IS



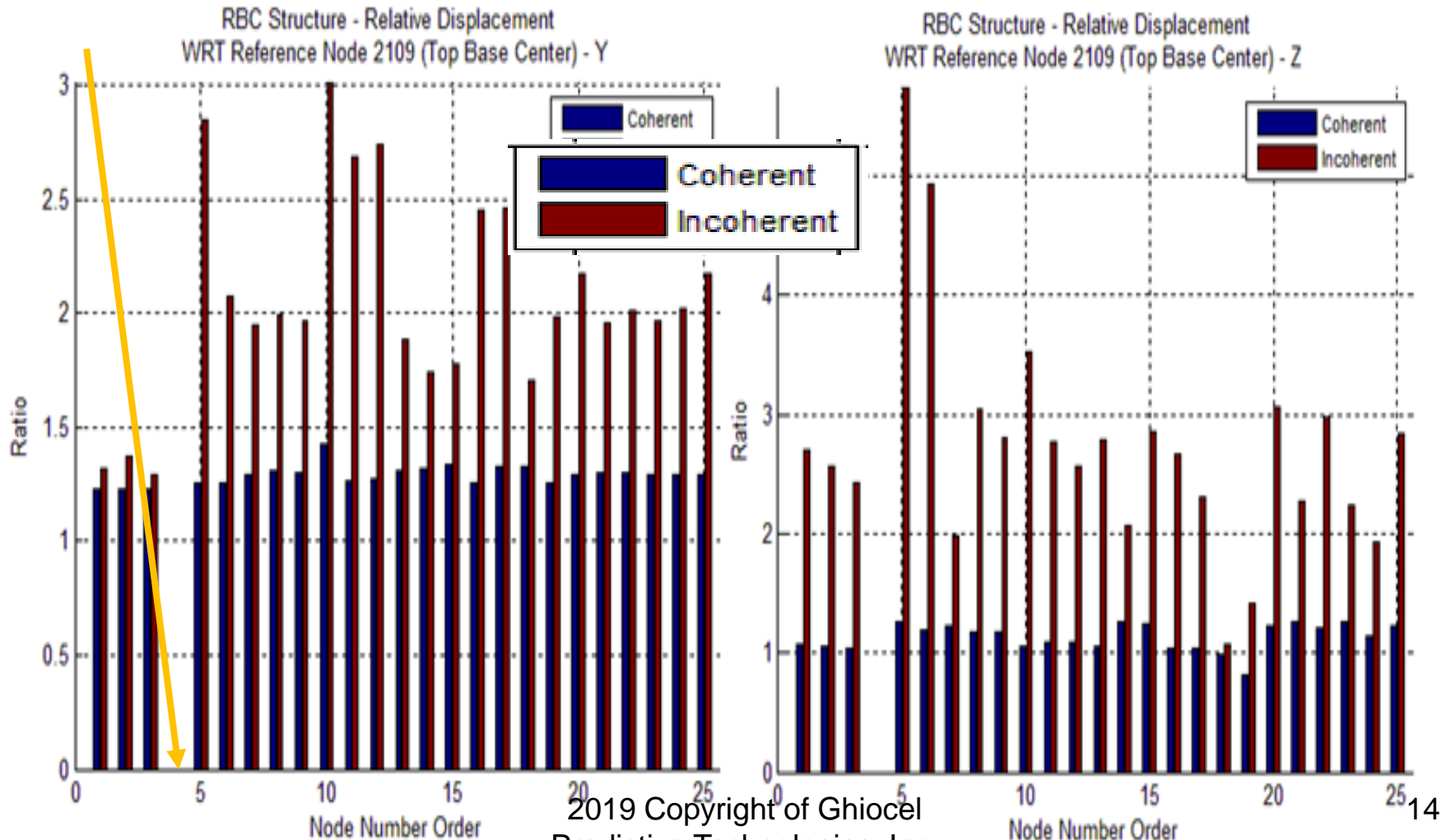
Vertical

RBC (Medium Soil, With Isolators) – ARS (Node 15471)
Direction Z at Top of IS



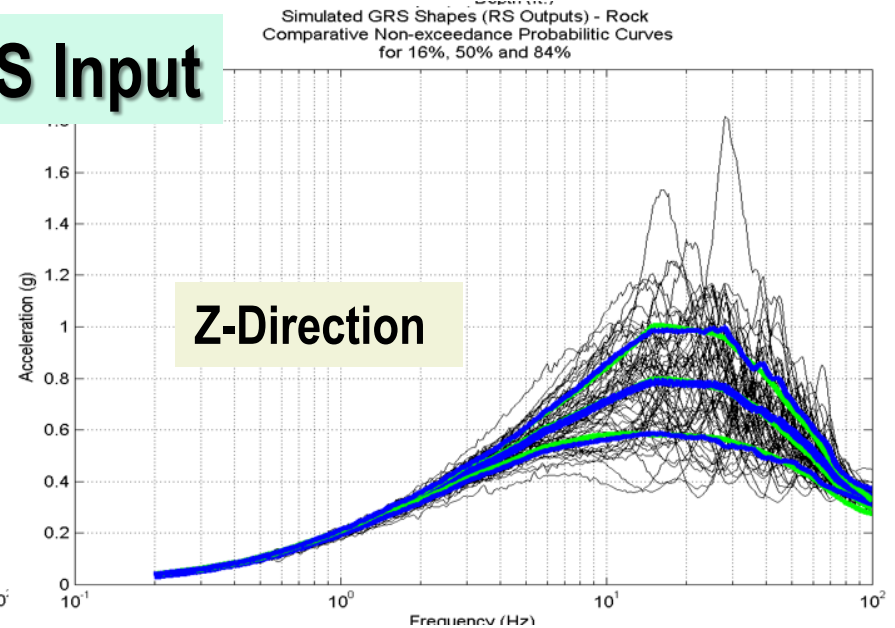
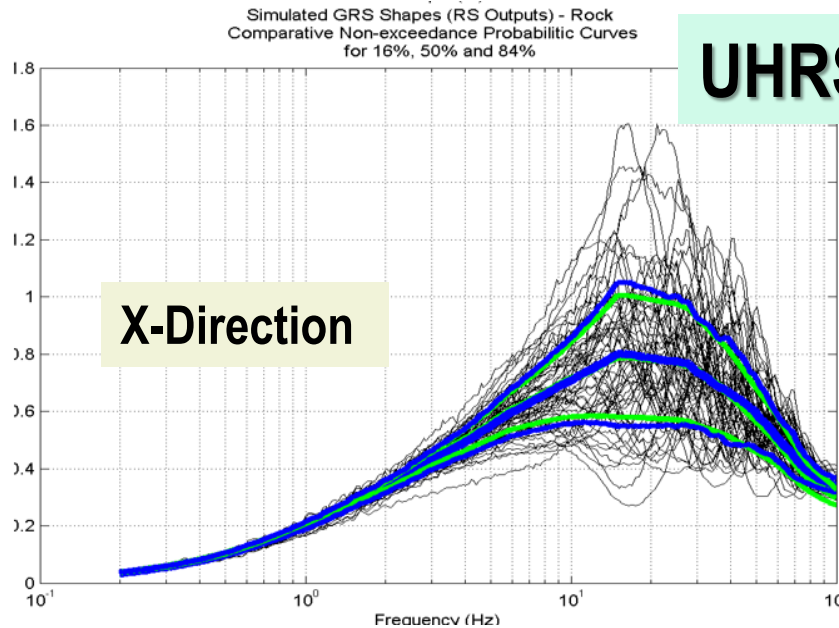
Effect of Motion Incoherency on Relative Displacements at NI Complex Critical Locations

Reference Location is Top Slab Center

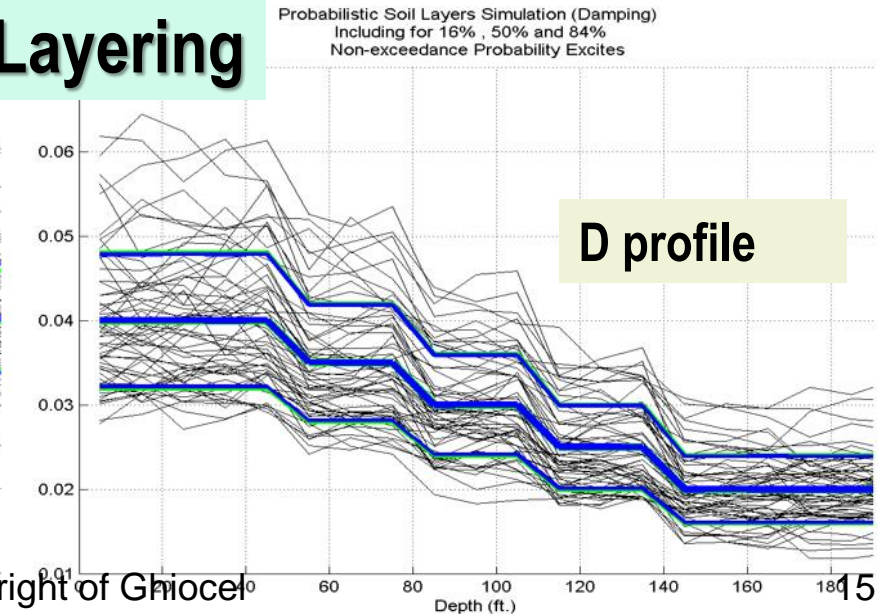
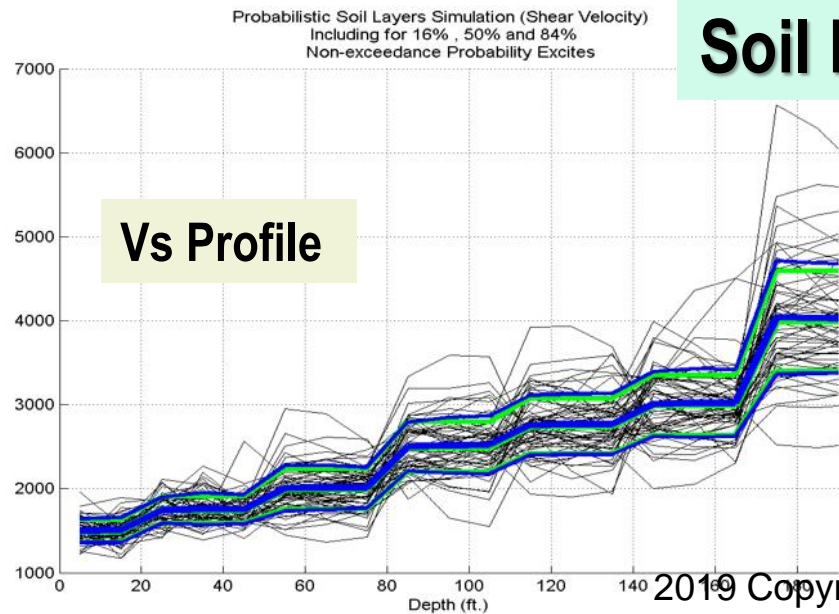


3. Probabilistic vs. Deterministic SSI Responses

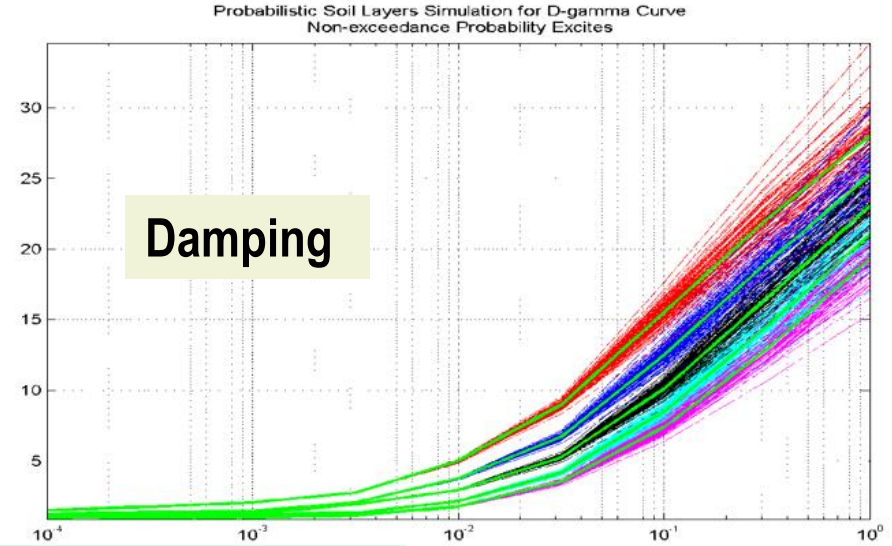
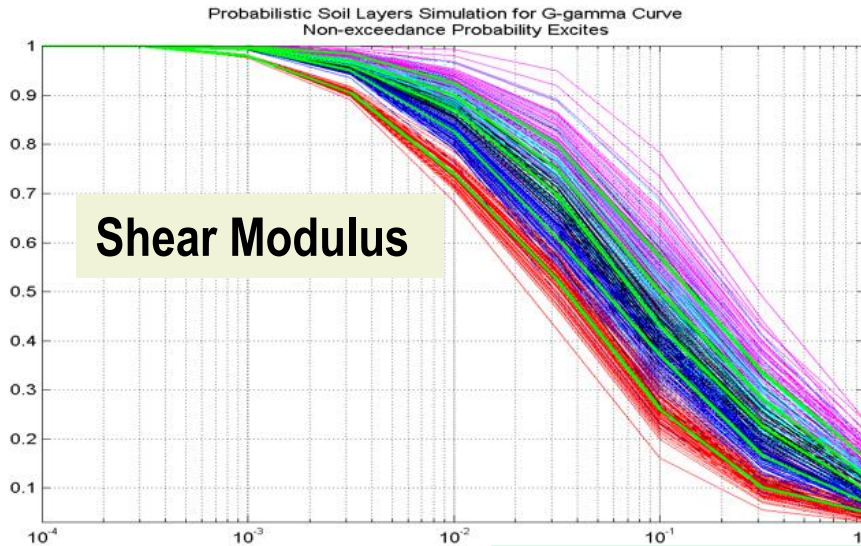
UHRS Input



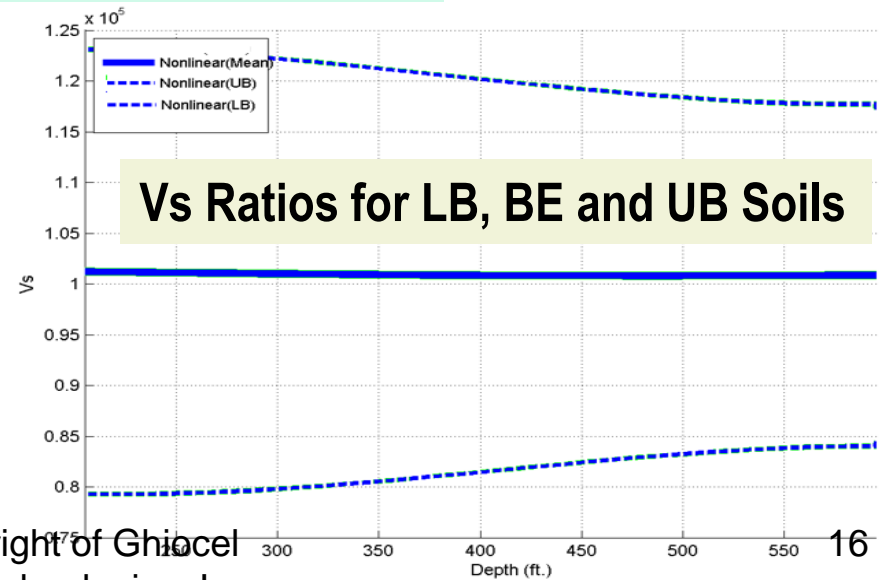
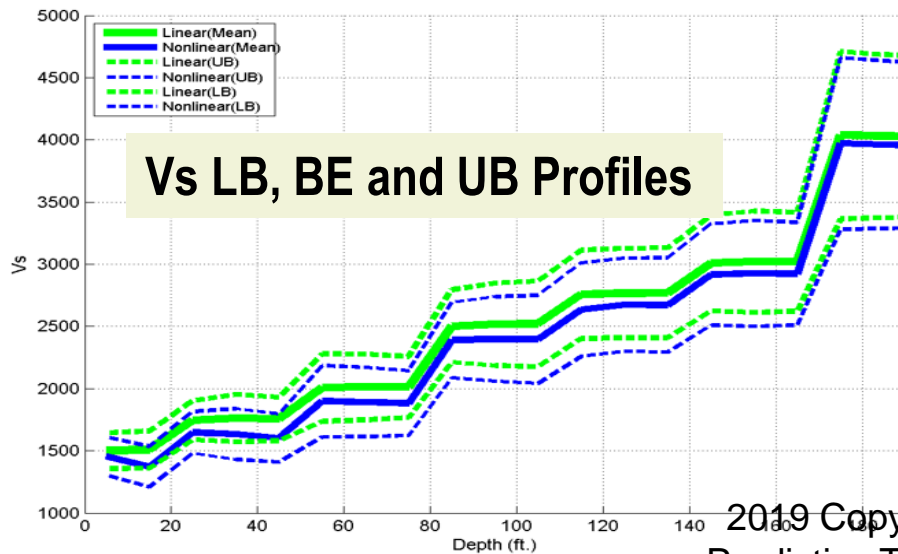
Soil Layering



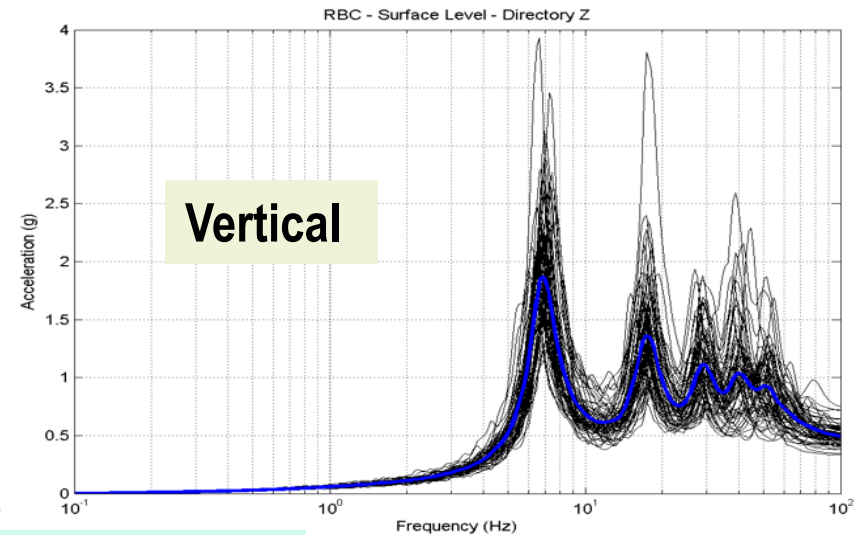
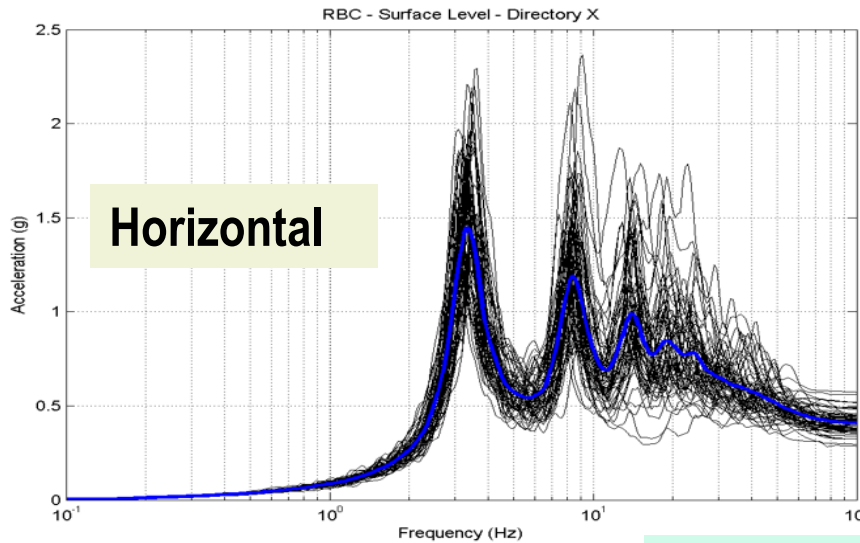
Soil Material Curves



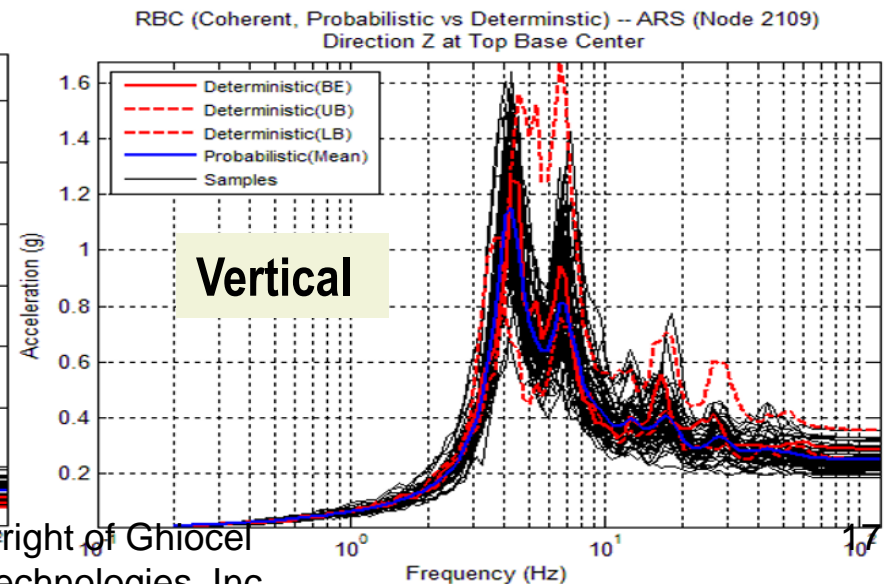
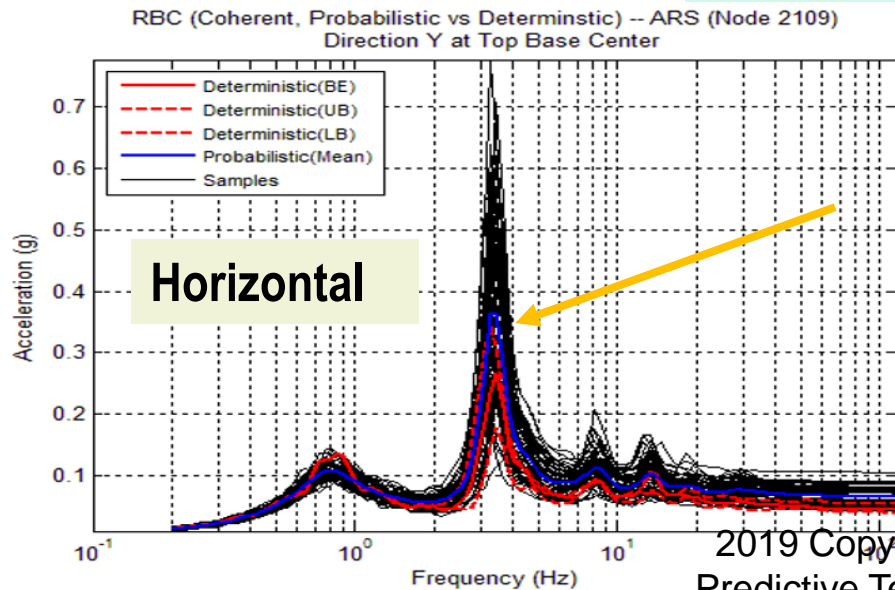
Deterministic Soil Profiles



Surface GRS

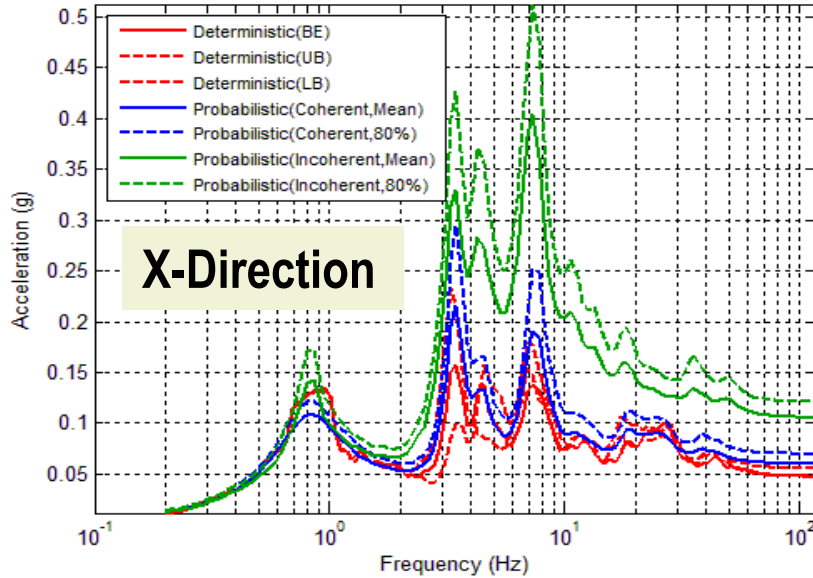


Top Base Center

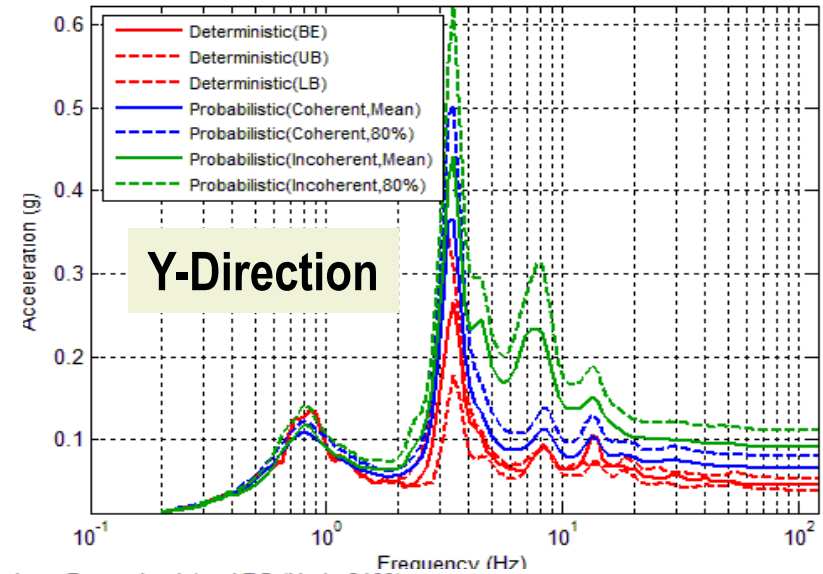


Probabilistic-Deterministic ISRS for NI Complex

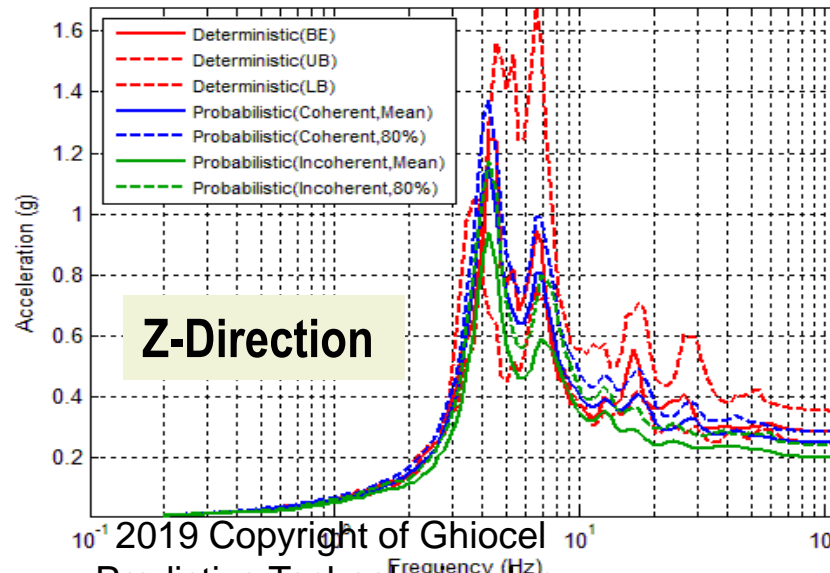
RBC (Probabilistic vs Deterministic) -- ARS (Node 2109)
Direction X at Top Base Center



RBC (Probabilistic vs Deterministic) -- ARS (Node 2109)
Direction Y at Top Base Center



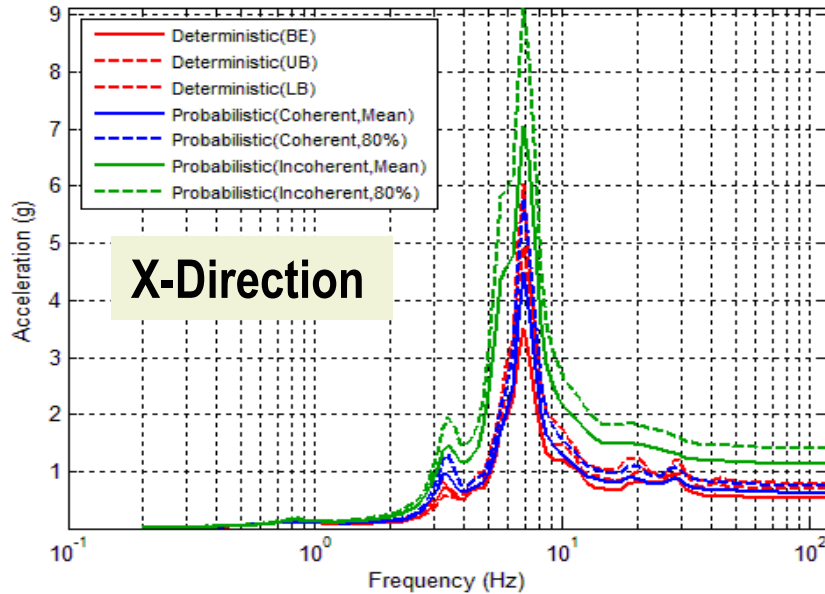
RBC (Probabilistic vs Deterministic) -- ARS (Node 2109)
Direction Z at Top Base Center



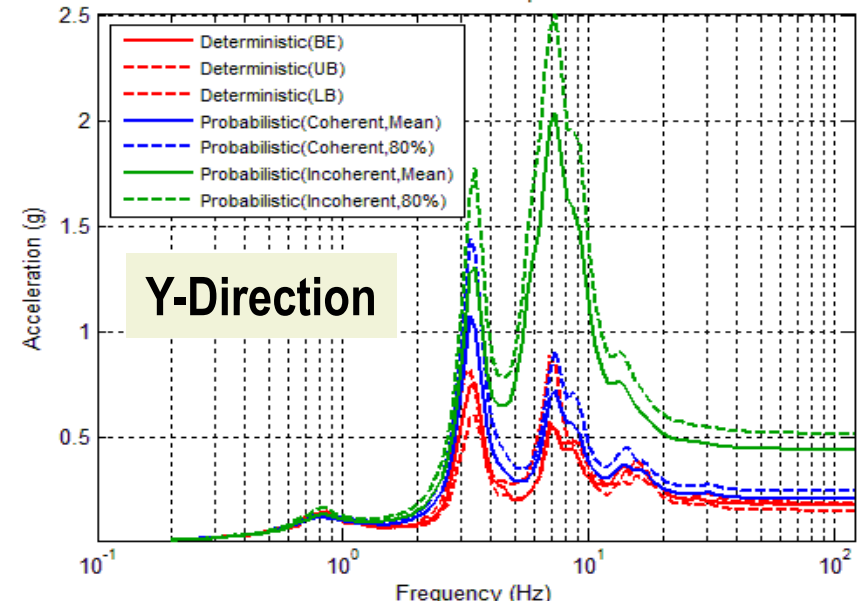
Top Base Center

Probabilistic-Deterministic ISRS for NI Complex

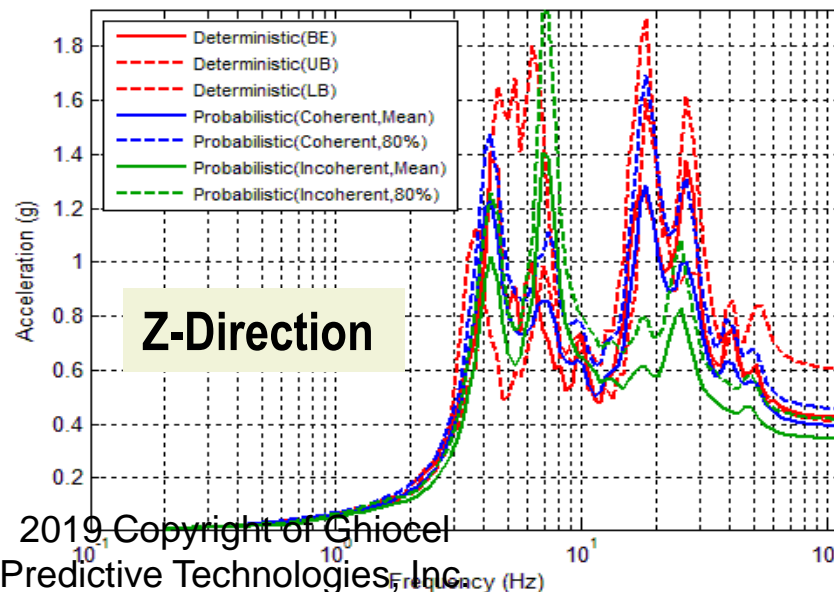
RBC (Probabilistic vs Deterministic) -- ARS (Node 15471)
Direction X at Top of IS



RBC (Probabilistic vs Deterministic) -- ARS (Node 15471)
Direction Y at Top of IS



RBC (Probabilistic vs Deterministic) -- ARS (Node 15471)
Direction Z at Top of IS



Some Remarks from 2015 Studies:

- Probabilistic SSI analysis results are significantly larger than Deterministic SSI analysis results for coherent inputs.
- Probabilistic SSI analysis produces significantly larger ISRS amplifications for higher frequency modes.
- Motion incoherency increases significantly the relative displacements within the NI complex
- LRB isolator axial forces are largely increased due to motion incoherency (*not shown*)

4. Frequency-Dependent 3D HVD isolators

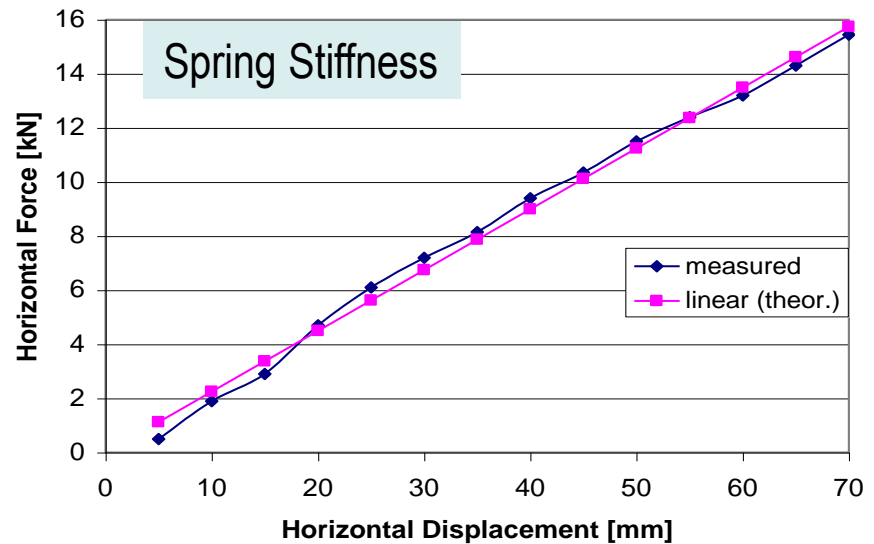
GERB BCS

2019 Studies

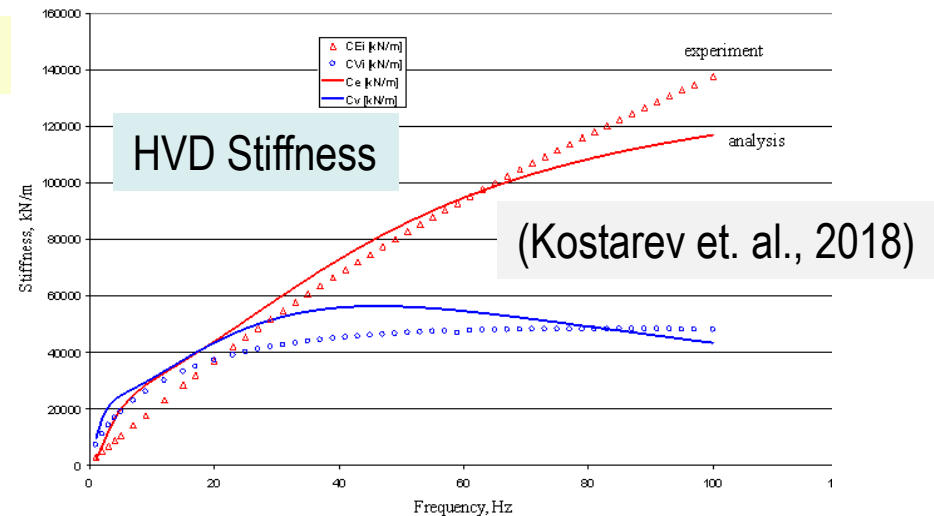
3D Springs



(Nawrotzki et al., 2018)



3D HV Dampers



3D HVD is a new ACS SASSI element

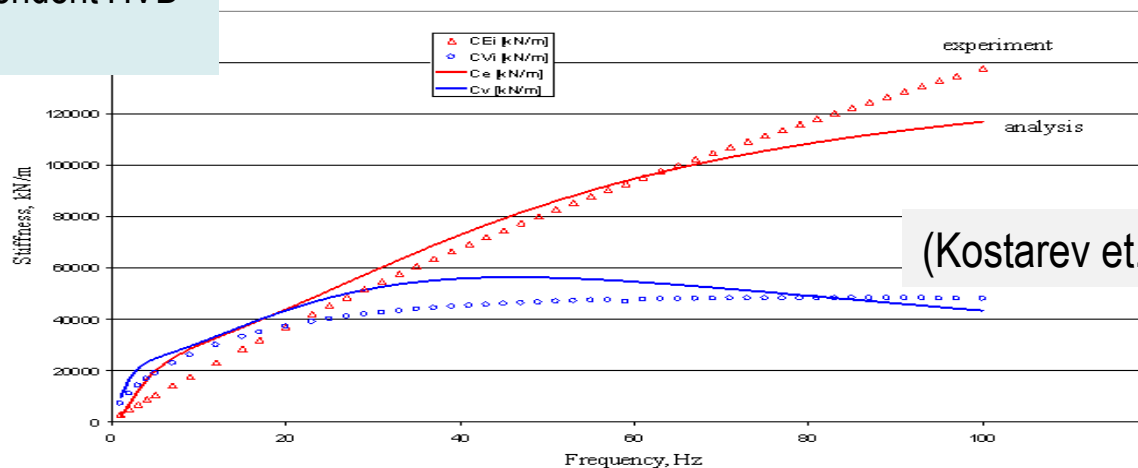
3-Node HVD Element is Based on 4-Parameter Maxwell Model

GERB BCS/HVD



(Nawrotzki, Kostarev et al, 2018)

Analytical vs. Experimental
Frequency-Dependent HVD
Stiffnesses



(Kostarev et. al., 2018)

Chain 1

k_1

$$\omega_1 = \frac{k_1}{B_1}$$

B_1

Node 3

Node 3'

Node 2

Chain 2

k_2

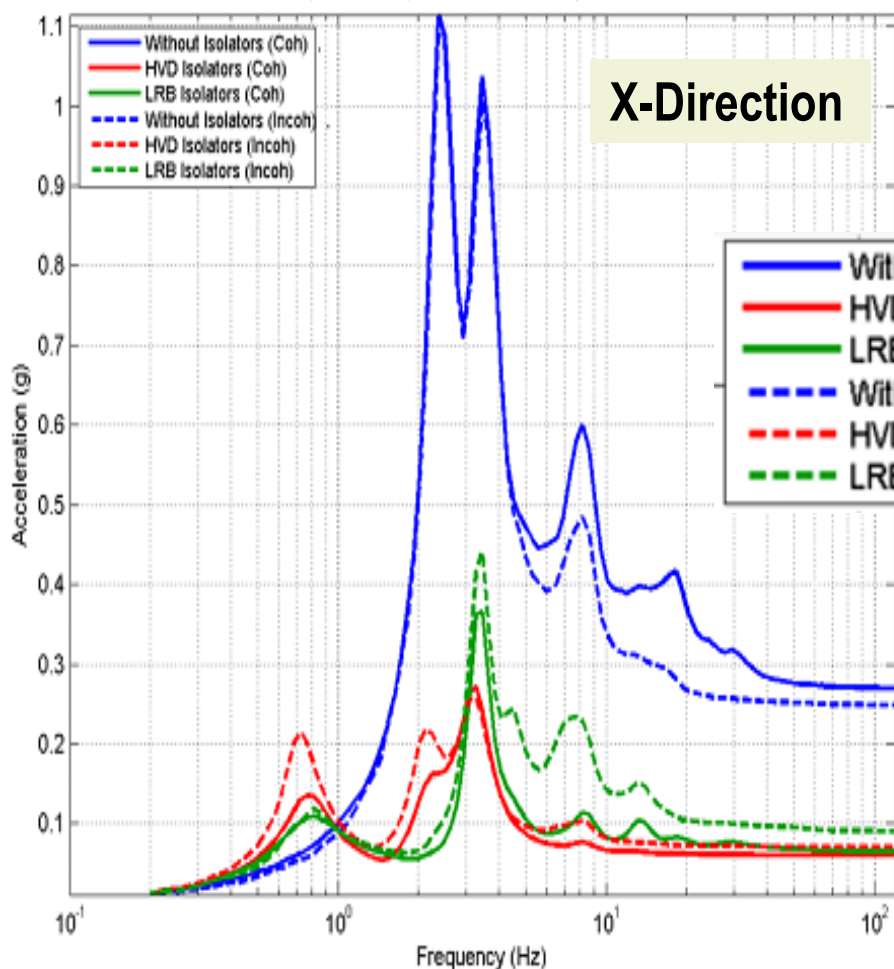
$$\omega_2 = \frac{k_2}{B_2}$$

B_2

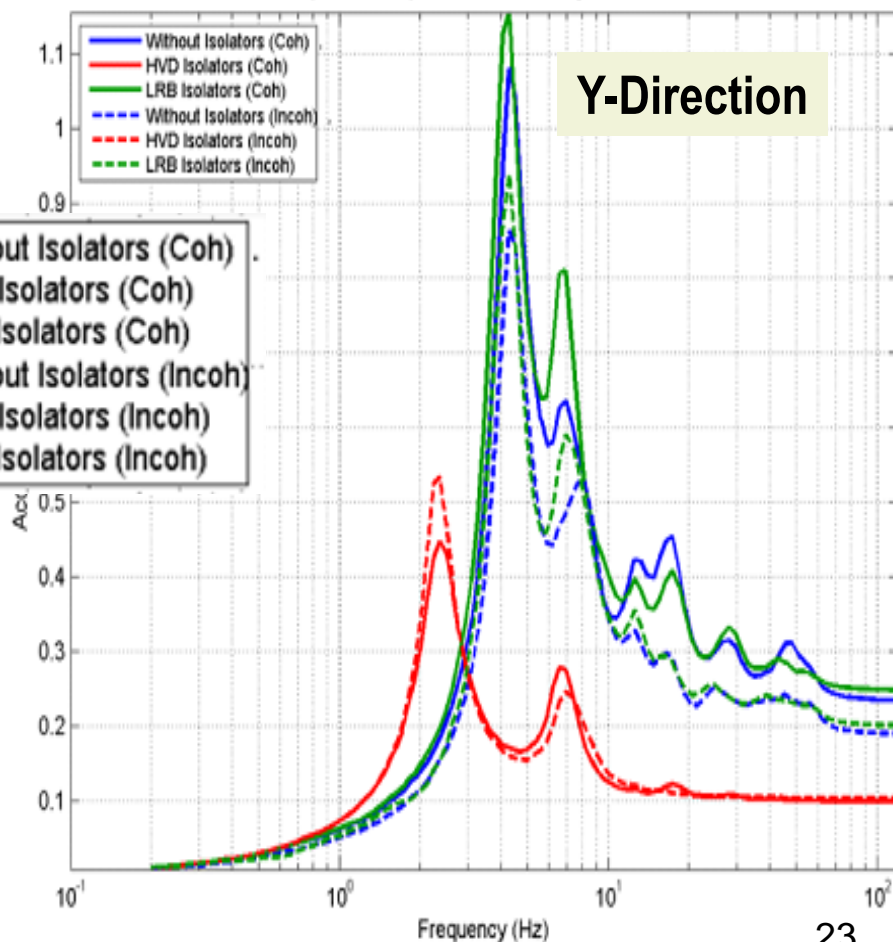
Comparative Coherent vs. Incoherent ISRS for No Isolators vs. HVD and LRB Isolators

Top Base Center

RBC (Coherent, Mean of 60 Simulations)
ARS (Node 2109) - Direction Y at Top Base Center

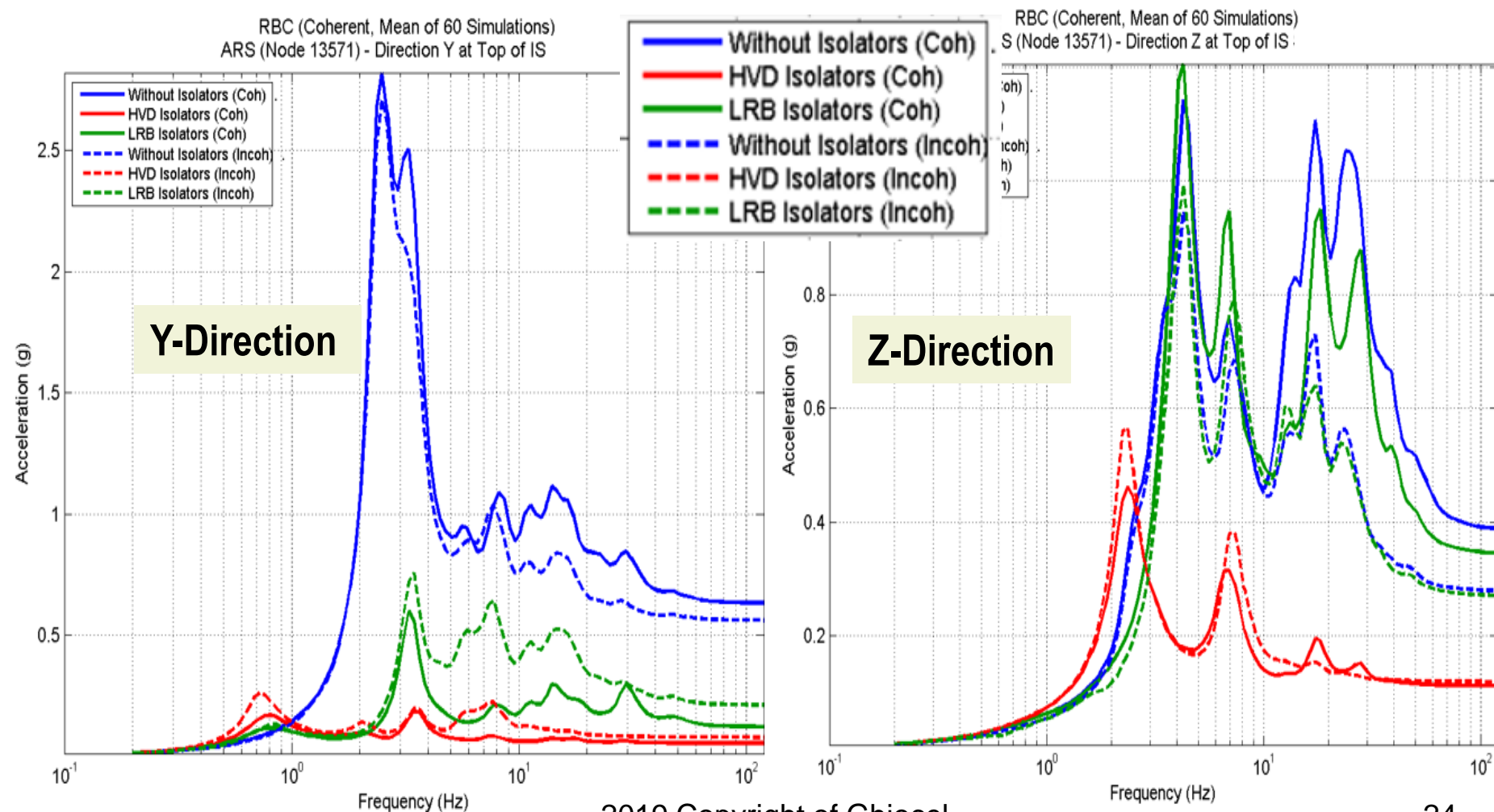


RBC (Coherent, Mean of 60 Simulations)
ARS (Node 2109) - Direction Z at Top Base Center



Comparative Coherent vs. Incoherent ISRS for No Isolators vs. HVD and LRB Isolators

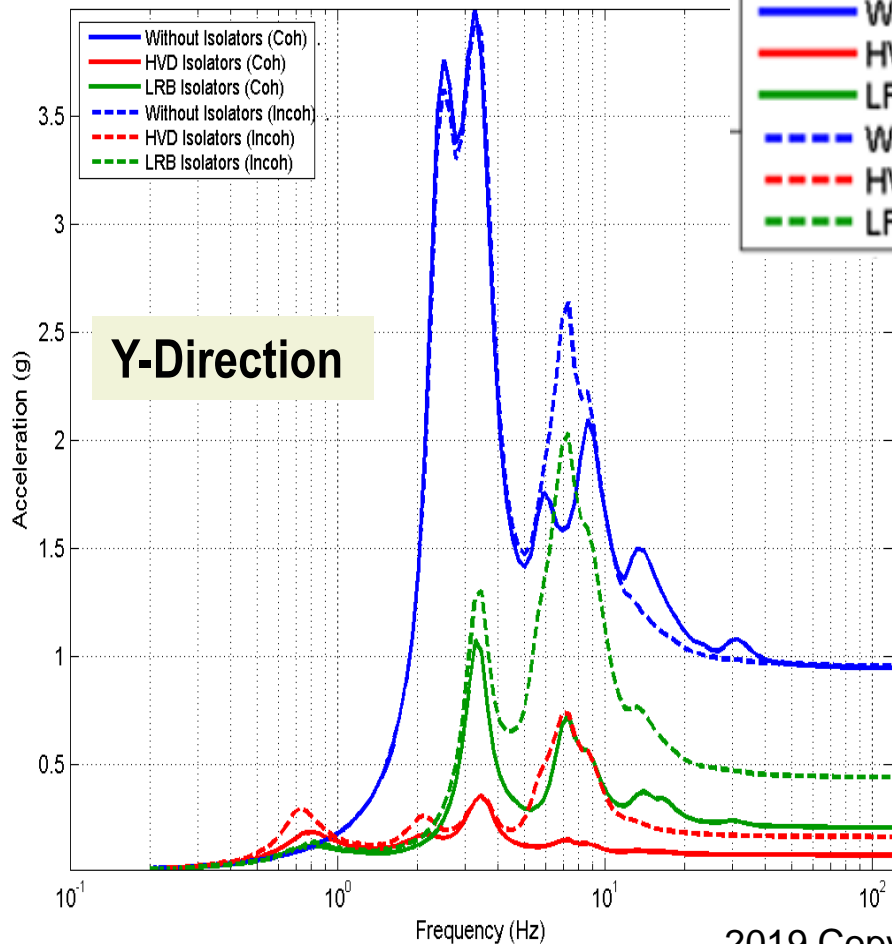
Top of IS near Center



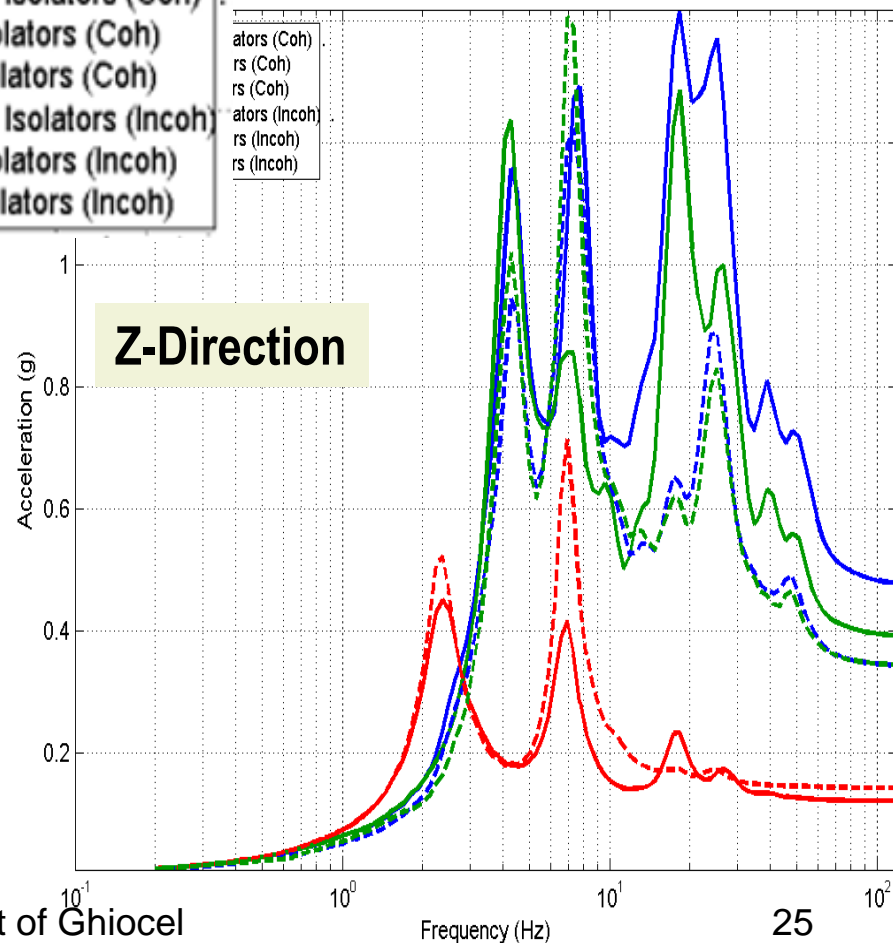
Comparative Coherent vs. Incoherent ISRS for No Isolators vs. HVD and LRB Isolators

Top of IS near Edge

RBC (Coherent, Mean of 60 Simulations)
ARS (Node 15471) - Direction Y at Top of IS



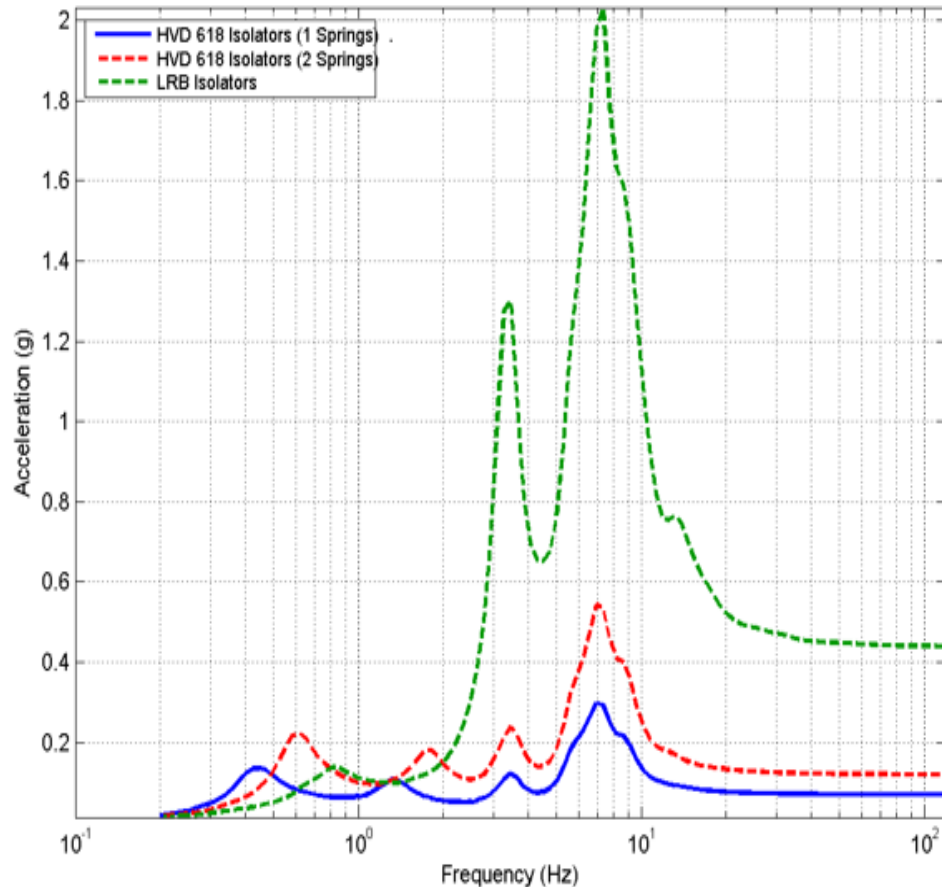
RBC (Coherent, Mean of 60 Simulations)
ARS (Node 15471) - Direction Z at Top of IS



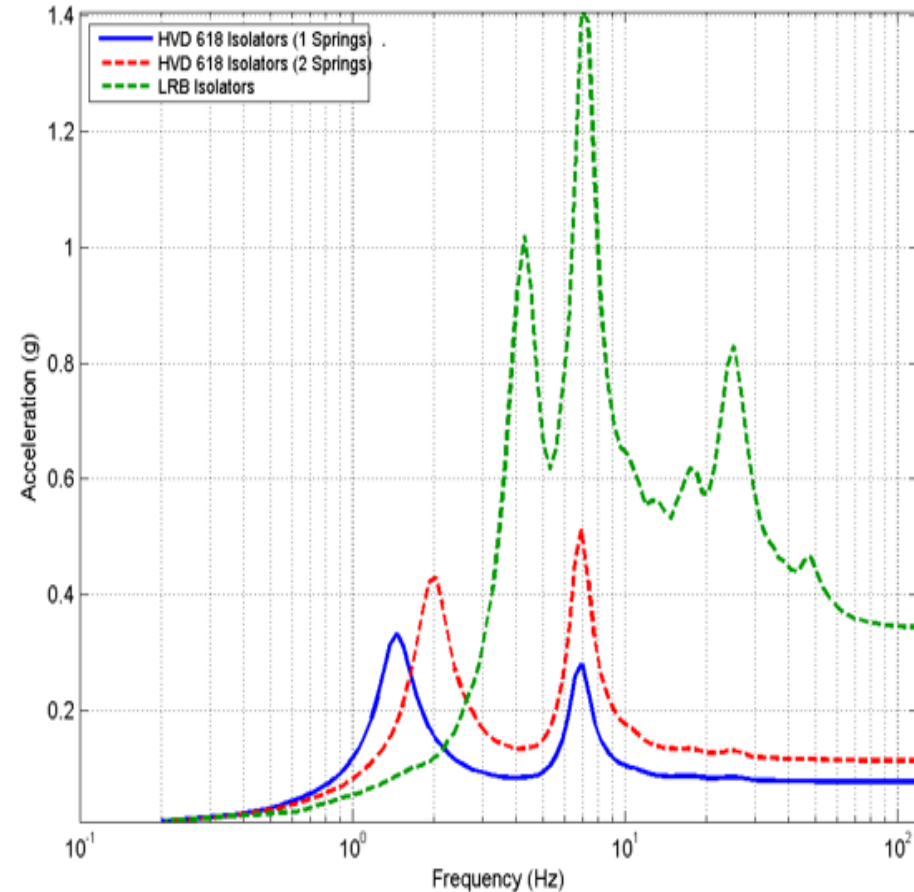
Coherent ISRS Using Different Number of Spring Units for HVD 1 and HVD 2 vs. LRB Isolators

Top of IS

RBC (Incoherent, Mean of 60 Simulations)
ARS (Node 15471) - Direction Y at Top of IS



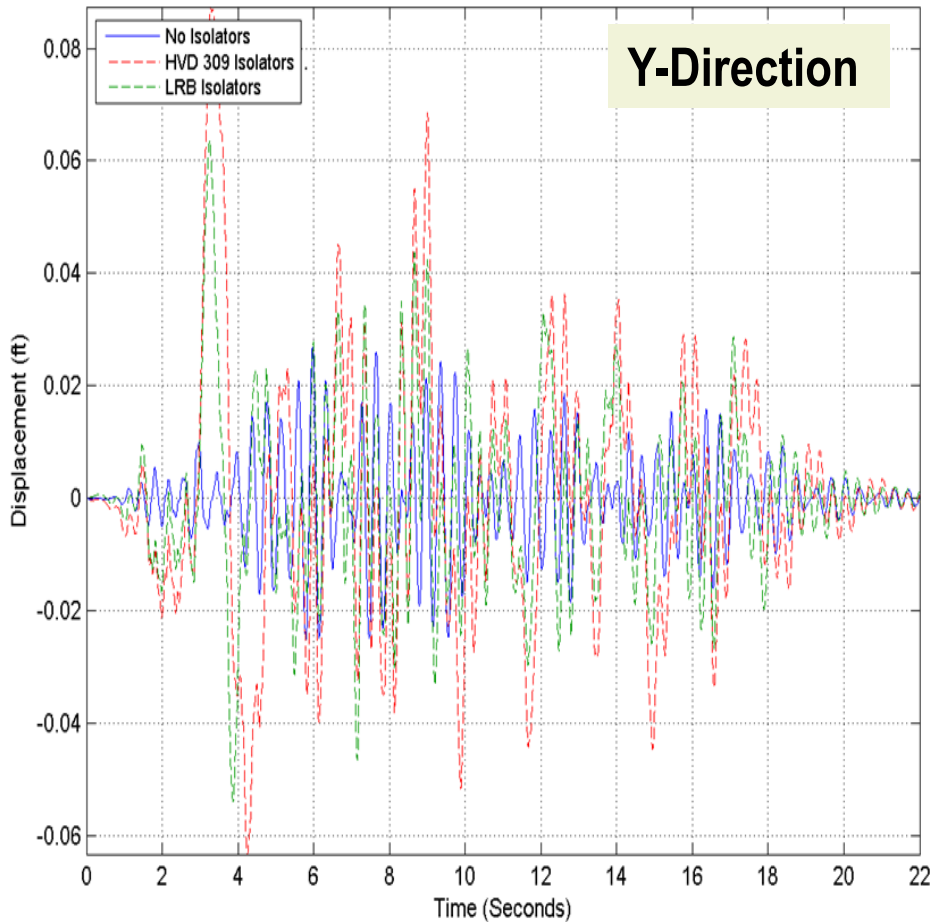
RBC (Incoherent, Mean of 60 Simulations)
ARS (Node 15471) - Direction Z at Top of IS



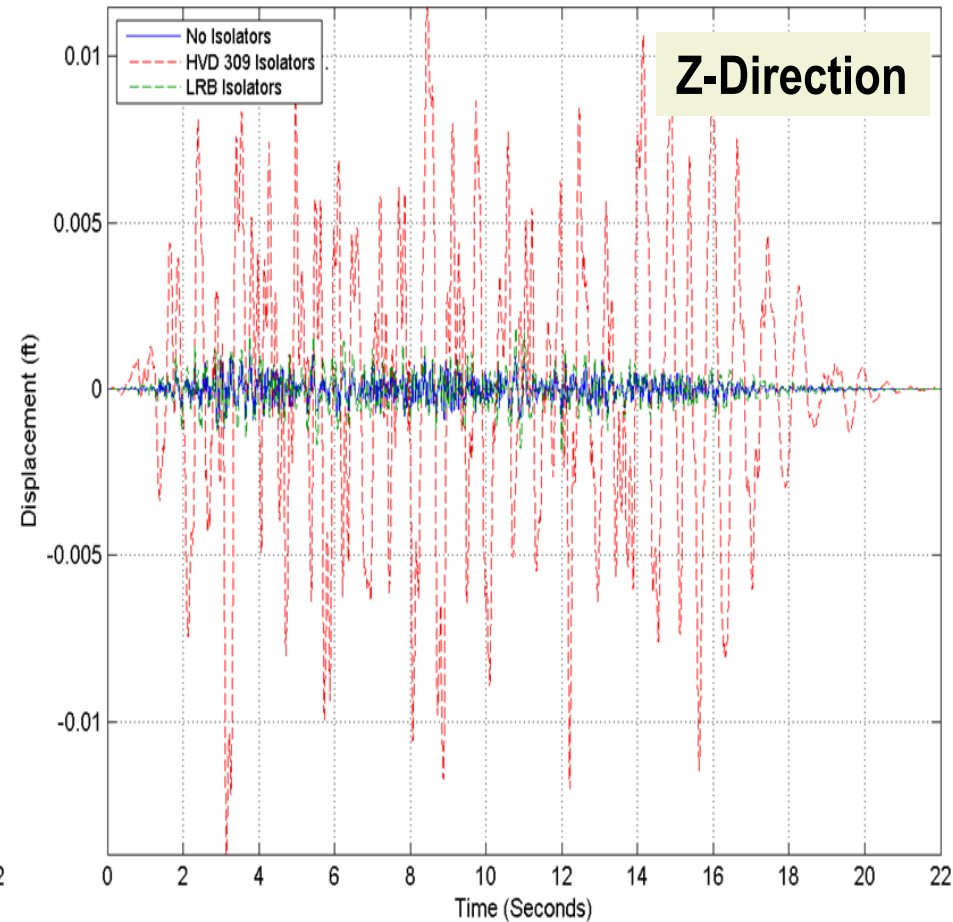
Comparative Coherent Relative Displacements wrt to Top Base Center

High Elevation Location

RBC (Coherent, Simulation 1)
THD (Node 16593)
Direction X



RBC (Coherent, Simulation 1)
THD (Node 16593)
Direction Z



CONCLUDING REMARKS

The main conclusions are:

- i) the RB complex base-isolation is highly effective for both the rock and soil sites,
- ii) the motion incoherency largely amplifies the horizontal ISRS and relative displacements within NI complex,
- iii) the 3D HVD isolators are more effective than the 2D LRB isolators, especially for the vertical motions.